Mass Estimating Relations

- Lecture #6 September 14, 2023
- Review of iterative design approach
- Mass Estimating Relations (MERs)
- Sample vehicle design analysis Picking projects and specialties for ENAE 484



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Akin's Laws of Spacecraft Design - #3

Design is an iterative process. The necessary number of iterations is one more than the number you have currently done. This is true at any point in time.

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Overview of the Design Process

Program Objectives System Requirements

Vehicle-level Estimation (based on a few parameters from prior art)

Increasing complexity

Increasing accuracy

Decreasing ability to comprehend the "big picture"



Basic Axiom: Relative rankings between competing systems will remain consistent from level to level

System-level Estimation (system parameters based on prior experience)

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System-level Design (based on disciplineoriented analysis)



Vehicle-Level Prelim Design - 1st Pass

- Single Stage to Orbit (SSTO) vehicle
- $\Delta V = 9200 \text{ m/sec}$
- 5000 kg payload
- LOX/LH2 propellants

- Isp=430 sec (Ve=4214 m/sec) $- \delta = 0.08$



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$r = e^{-\frac{\Delta V}{Ve}} = 0.1127$

$\lambda = r - \delta = 0.0327$

$M_o = \frac{M_\ell}{\lambda} = 153,000 \ kg$

$M_i = \delta M_o = 12,240 \ kg$

 $M_p = M_o(1-r) = 135,800 \ kg$



System-Level Estimation

• Start with propellant tanks (biggest part) • LOX/LH2 engines generally run at mixture ratio of 6:1 (by weight) – LH2: 19,390 kg – LOX: 116,400 kg • Propellant densities

 $\rho_{LOX} = 1140 \ \frac{kg}{m^3}$

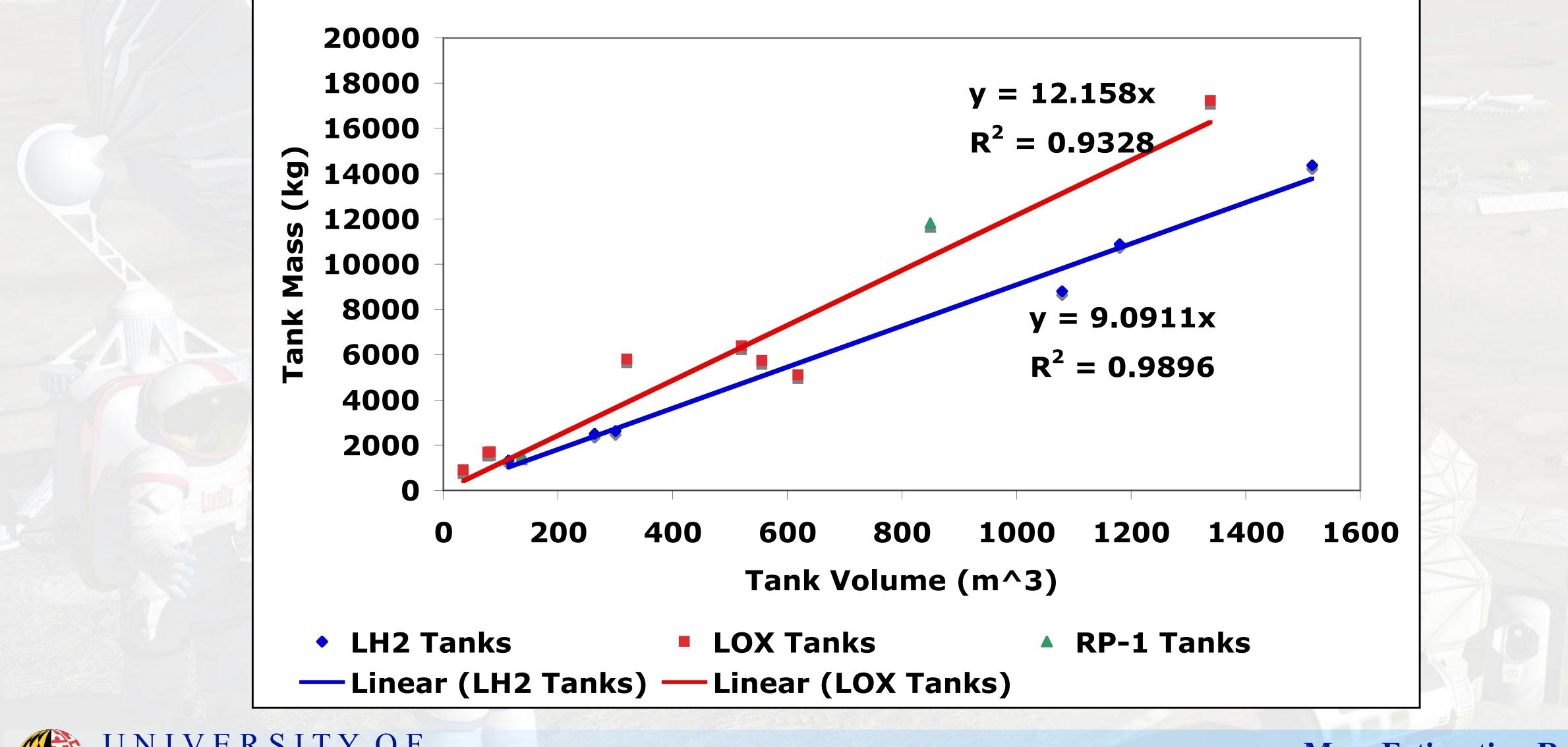


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$\rho_{LH_2} = 71 \ \frac{kg}{m^3}$



Propellant Tank Regression Data



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Propellant Tank MERs (Volume)

• LH₂ tanks

 $M_{LH_2} T_{ank} \langle kg \rangle = 9.09 V_{LH_2} \langle m^3 \rangle$

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• All other tanks (e.g., LOX, RP-1, LCH₄, hypergols) $M_{Tank}\langle kg\rangle = 12.16V_{prop}\langle m^3\rangle$





Propellant Tank MERs (Mass) • LH₂ tanks $ho_{LH_2} = 71 \ \frac{kg}{m^3} \Longrightarrow M_{LH_2} \ _{Tank}\langle kg \rangle = 0.128 M_{LH_2} \langle kg \rangle$ • LOX tanks $\rho_{LOX} = 1140 \frac{kg}{m^3} \Longrightarrow M_{LOX \ Tank} \langle kg \rangle = 0.0107 M_{LOX} \langle kg \rangle$ • RP-1 tanks $\rho_{RP1} = 820 \frac{kg}{m^3} \longrightarrow M_{RP1 \ Tank} \langle kg \rangle = 0.0148 M_{RP1} \langle kg \rangle$ • LCH₄ tanks $\rho_{LCH_4} = 423 \ \frac{kg}{m^3} \implies M_{LCH_4 \ Tank} \langle kg \rangle = 0.0287 \ M_{LCH_4} \langle kg \rangle$



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Cryogenic Insulation MERs





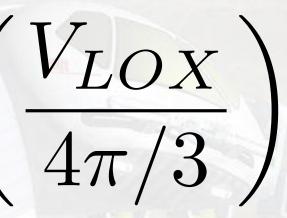
9

 M_{LH_2} Insulation $\langle kg \rangle = 2.88A_{tank} \langle \frac{kg}{m^2} \rangle$

 M_{LOX/LCH_4} Insulation $\langle kg \rangle = 1.123 A_{tank} \langle \frac{kg}{m^2} \rangle$



LOX Tank Design • Mass of LOX=116,400 kg



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 $M_{LOX Tank} = 0.0107(116, 400) = 1245 \ kg$ Need area to find LOX tank insulation mass - assume a sphere $V_{LOX \ Tank} = \frac{M_{LOX}}{\rho_{LOX}} = 102.1 \ m^3$ $r_{LOX \ Tank} = \left(\frac{V_{LOX}}{4\pi/3}\right)^{\frac{1}{3}} = 2.90 \ m$ $A_{LOX Tank} = 4\pi r^2 = 105.6 m^2$ $M_{LOX Insulation} = 1.123 \langle \frac{kg}{m^2} \rangle (105.6 \langle m^2 \rangle) = 119 \ kg$



LH₂ Tank Design • Mass of LH₂=19,390 kg $M_{LH_2} T_{ank} \langle kg \rangle = 0.128(19, 390) = 2482 \ kg$

• Again, assume LH₂ tank is spherical

 $r_{LH_2 Tank} = \left(\frac{V_{LH_2}}{4\pi/3}\right)^{\frac{1}{3}} = 4.02 m$

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 $A_{LH_2 Tank} = 4\pi r^2 = 203.6 \ m^2$ $M_{LH_2 \ Insulation} = 2.88 \left\langle \frac{kg}{m^2} \right\rangle (203.6 \left\langle m^2 \right\rangle) = 586 \ kg$

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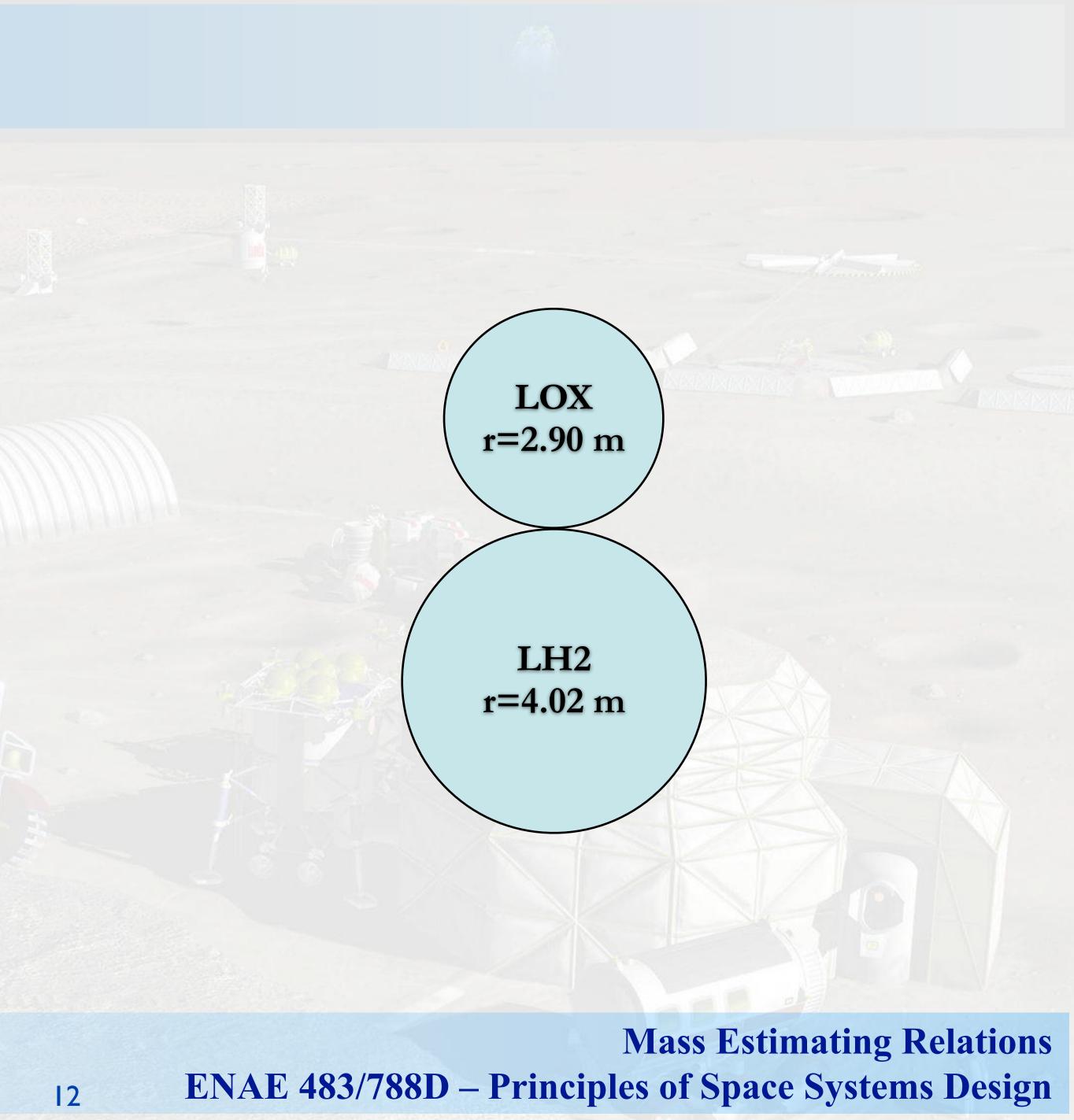
$V_{LH_2 Tank} = \frac{M_{LH_2}}{\rho_{LH_2}} = 273.1 \ m^3$



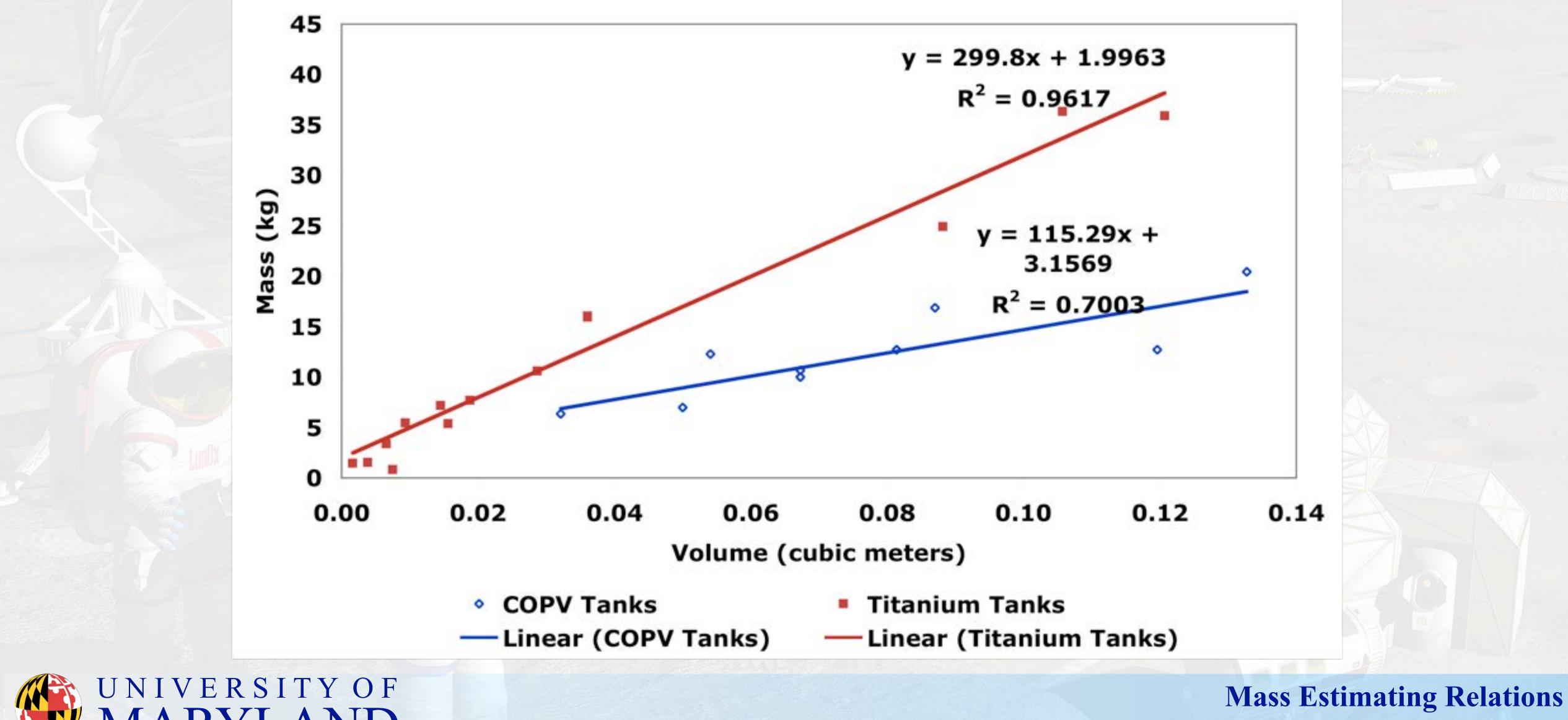
Current Design Sketch

• Masses – LOX Tank 1245 kg - LOX Tank Insulation 119 kg – LH₂ Tank 2482 kg – LH₂ Tank Insulation 586 kg





High-Pressure Gas Tanks





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Pressurized Gas Tank MERs

• COPV (Composite Overwrapped Pressure Vessel)

• Titanium tank



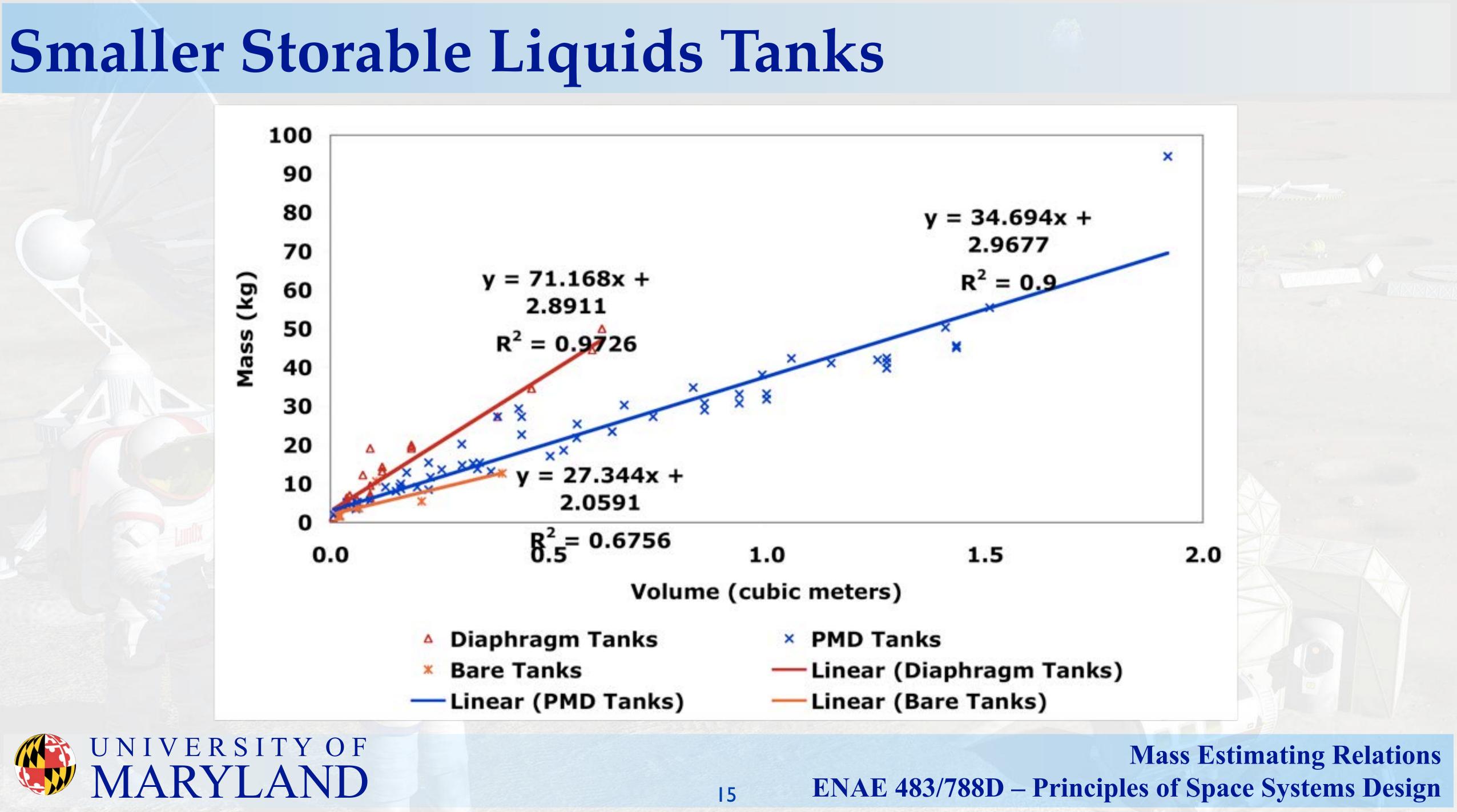


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$M_{COPV Tank}(kg) = 115.3 V_{contents}(m^3) + 3$

$M_{Ti Tank}(kg) = 299.8 V_{contents}(m^3) + 2$





Small Liquid Tankage MERs

- Bare metal tanks
- Tanks with propellant management devices
- Titanium tanks with positive expulsion bladders



$M_{Bare\ Tank}(kg) = 27.34\ V_{contents}(m^3) + 2$

$M_{PMD Tank}(kg) = 34.69 V_{contents}(m^3) + 3$

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$M_{Diaphragm\ Tank}(kg) = 71.17\ V_{contents}(m^3) + 3$



Minimum Cost Lunar Architecture

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Orbital Maneuvering Stage (OMS)

- Gross mass 6950 kg
 - Inert mass 695 kg
 - Propellant mass 6255 kg
 - Mixture ratio $N_2O_4/UDMH = 2.0$ (by mass)
- N_2O_4 tank
 - Mass = 4170 kg
 - Density = 1450 kg/m^3
 - Volume $= 2.876 \text{ m}^3$
- UDMH tank
 - Mass = 2085 kg
 - Density = 793 kg/m^3
 - Volume = 2.629 m³

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N₂O₄ Tank Sizing

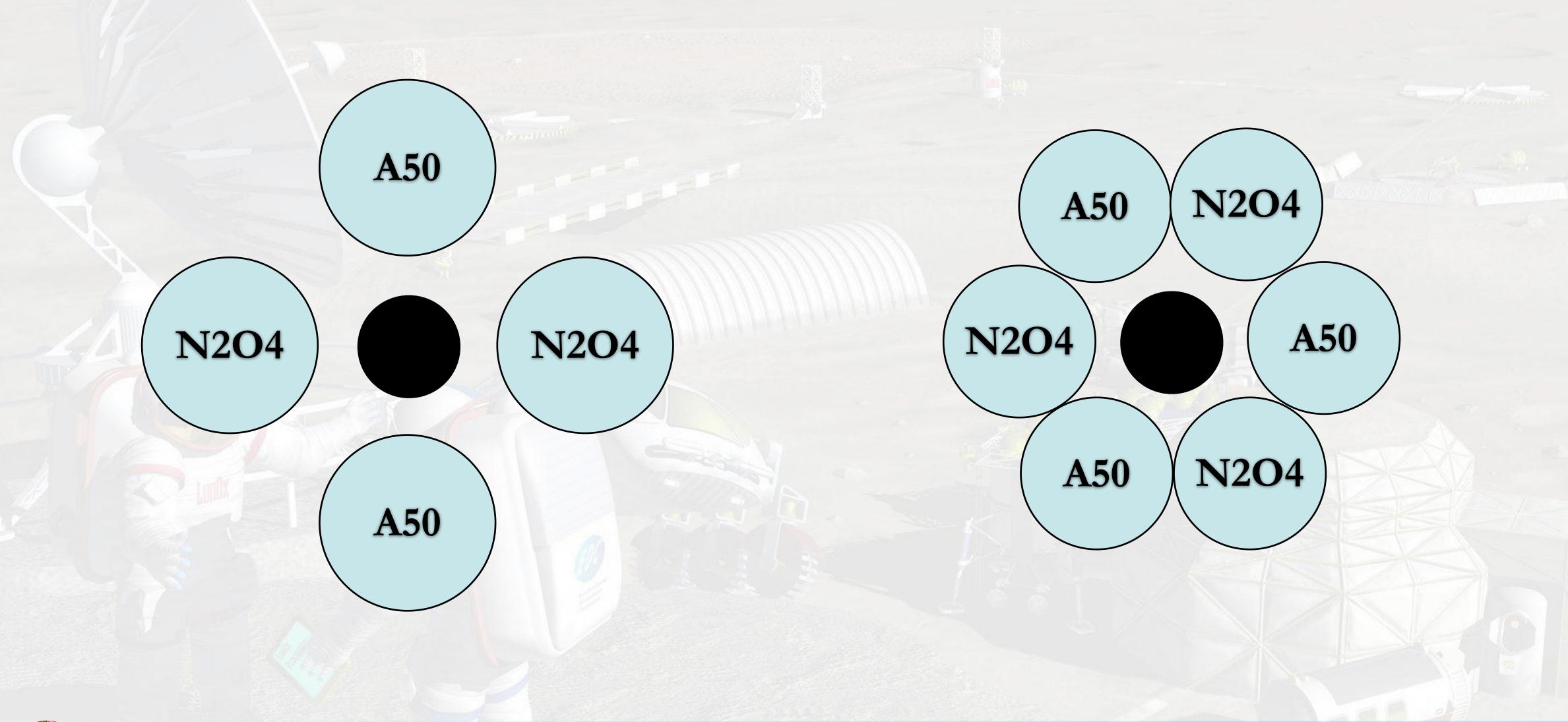
- Need total N_2O_4 volume = 2.876 m³
- Single PMD tank
 - -Radius = 0.882 m
 - Mass = 102.8 kg
- Dual PMD tanks
 - -Radius = 0.700 m
 - Mass = 52.9 kg (x2 = 105.8 kg)
- Triple PMD tanks
 - Radius = 0.612 m
 - Mass = 36.3 kg (x3 = 108.9 kg)

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Apollo LM Ascent Tank Configurations



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LM Ascent Stage Final Tank Configuration



0

N2O4

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UDMH



Other Structural MERs Fairings and shrouds

• Avionics

• Wiring



 $M_{fairing}\langle kg \rangle = 4.95 \left(A_{fairing} \langle m^2 \rangle \right)^{1.15}$

$M_{avionics}\langle kg \rangle = 10 \left(M_o \langle kg \rangle \right)^{0.361}$

$M_{wiring}\langle kg \rangle = 1.058\sqrt{M_o\langle kg \rangle}\ell^{0.25}$

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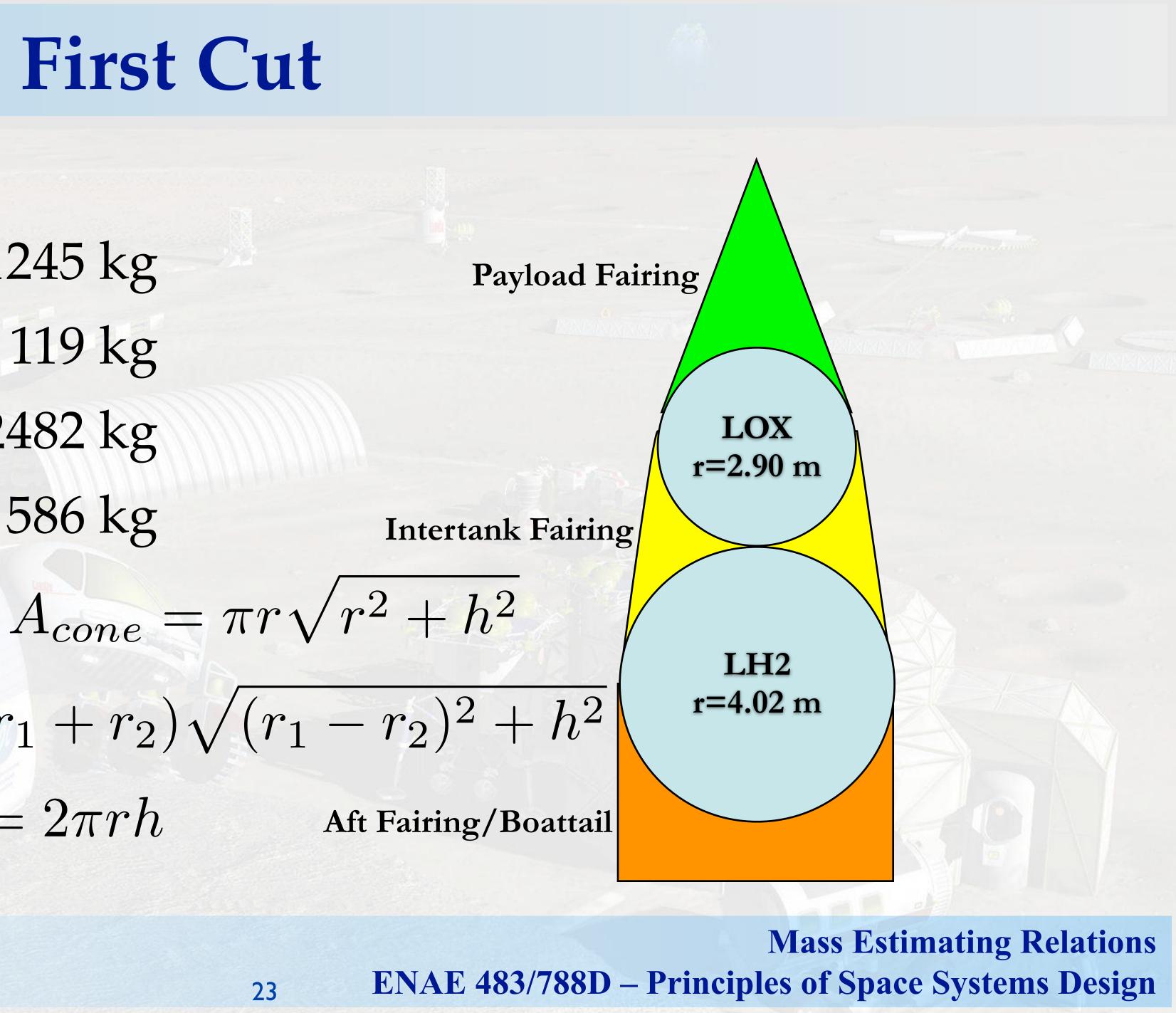
External Fairings - First Cut

• Masses – LOX Tank 1245 kg - LOX Tank Insulation 119 kg 2482 kg – LH₂ Tank – LH₂ Tank Insulation 586 kg

 $A_{frustrum} = \pi (r_1 + r_2) \sqrt{(r_1 - r_2)^2 + h^2}$

 $A_{cylinder} = 2\pi rh$



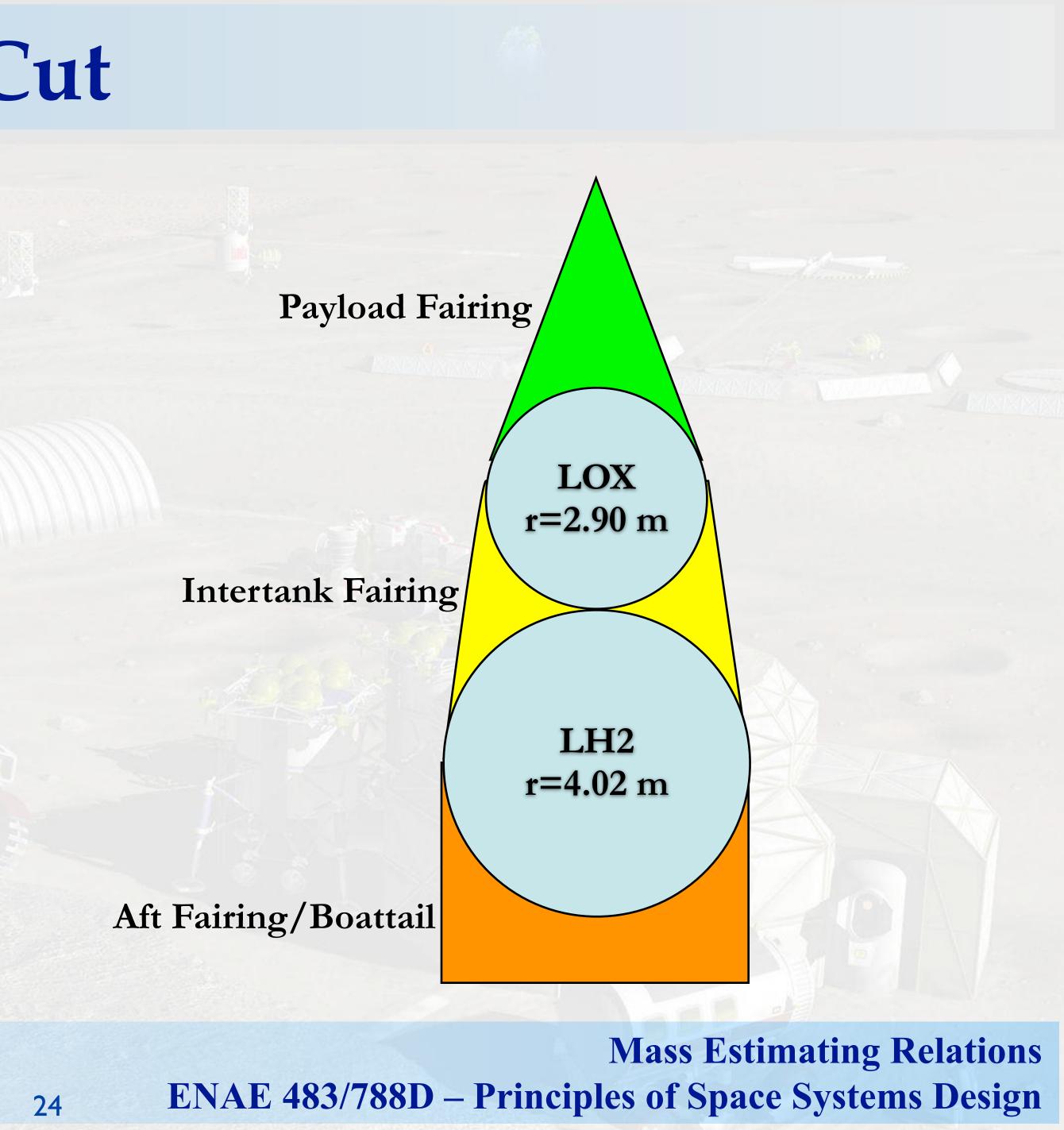


External Fairings - First Cut

 Assumptions – P/L fairing *b* - P/L fairing r– I/T fairing *h* -I/T fairing r_1 - I/T fairing r_2 – Aft fairing *h* – Aft fairing *r*

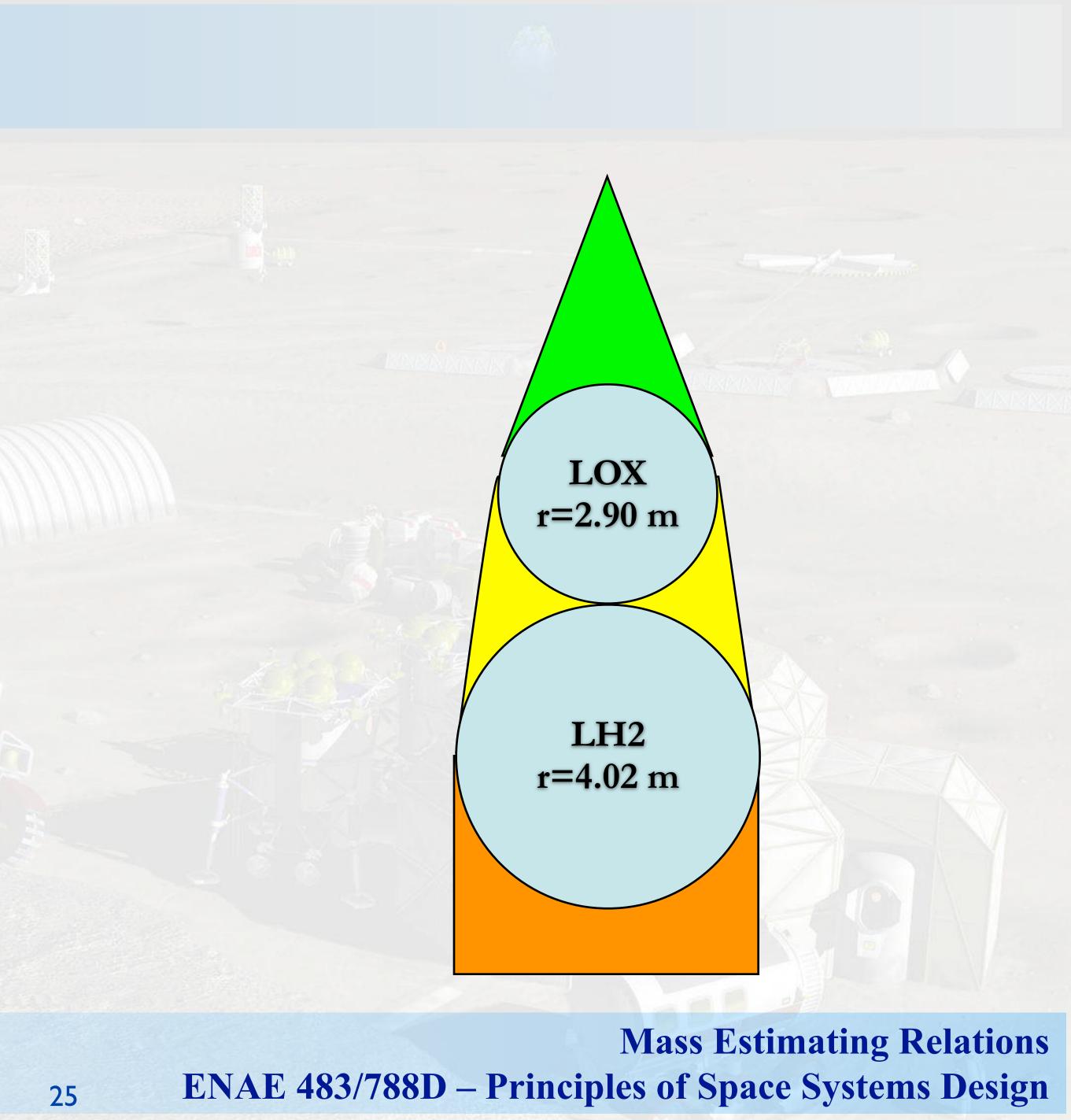
7 m 2.9 m 7 m 4.02 m 2.9 m 7 m 4.02 m





Fairing Analysis Payload Fairing 69.03 m² – Area 645 kg – Mass Intertank Fairing – Area 154.1 m^2 1624 kg – Mass • Aft Fairing 176.8 m^2 – Area 1902 kg – Mass

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Avionics and Wiring Masses

Avionics



$M_{wiring} \langle kg \rangle = 1.058 \sqrt{153,000} (21 \ m)^{0.25} = 886 \ kg$

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$M_{avionics} \langle kg \rangle = 10 \ (153, 000)^{0.361} = 744 \ kg$



Propulsion MERs

Liquid Pump-Fed Rocket Engine Mass $M_{Rocket Engine}(kg) = 7.81 \times 10^{-4} T(N) +$ $3.37 \times 10^{-5} T(N) \sqrt{\frac{A_e}{A} + 59}$

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Solid Rocket Motor Thrust Structure Mass



 $M_{Motor Casing} = 0.135 M_{propellants}$

$M_{Thrust Structure}(kg) = 2.55 \times 10^{-4} T(N)$



Propulsion MERs (continued)

• Gimbal Mass

• Gimbal Torque



 $M_{Gimbals}(kg) = 237.8 \left[\frac{T(N)}{P_0(Pa)} \right]^{.9375}$

$\tau_{Gimbals}(N \cdot m) = 990,000 \left[\frac{T(N)}{P_0(Pa)} \right]^{1.25}$

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Propulsion System Assumptions • Initial T/mg ratio = 1.3- Keeps final acceleration low with reasonable throttling • Number of engines = 6- Positive acceleration worst-case after engine out • Chamber pressure = 1000 psi = 6897 kPa Typical for high-performance LOX/LH2 engines • Expansion ratio $A_e/A_t=30$ Compromise ratio with good vacuum performance UNIVERSITY OF MARYLAND

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Propulsion Mass Estimates • Rocket Engine Thrust (each)

Rocket Engine Mass (each)

 $M_{Rocket Engine}(kg) = 7.81 \times 10^{-4}(324,900) +$

Thrust Structure Mass



 $T(N) = \frac{m_0 g(T/W)_0}{324,900} = 324,900 N$

n_{engines}

30

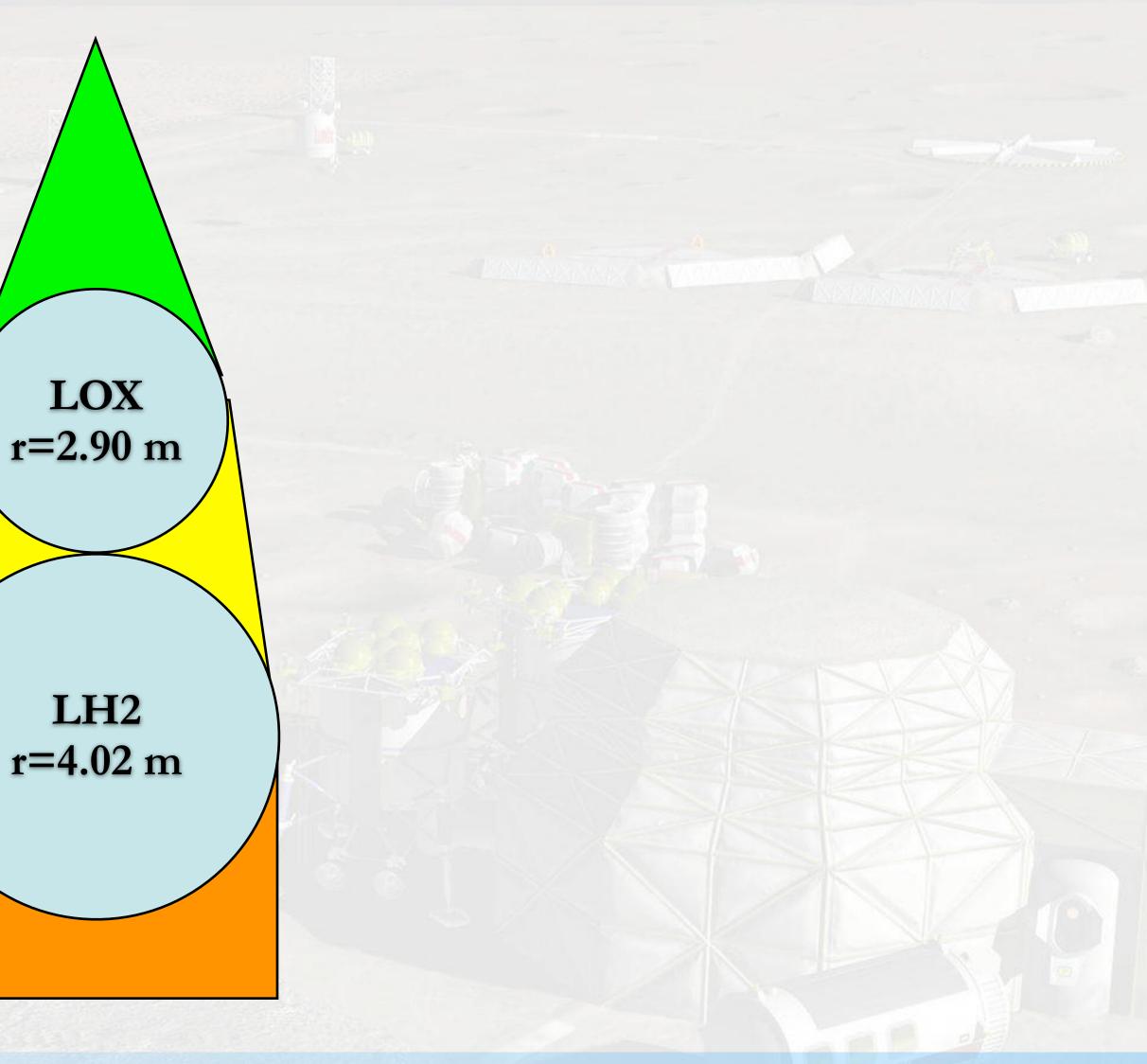
$3.37 \times 10^{-5}(324,900)\sqrt{30} + 59 = 373 \ kg$

$M_{Thrust Structure}(kg) = 2.55 \times 10^{-4}(324,900) = 82.8 \ kg$



First Pass Vehicle Configuration





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Mass Summary - First Pass

Initial Inert Mass Estimate LOX Tank LH2 Tank LOX Insulation LH2 Insulation Payload Fairing **Intertank Fairing** Aft Fairing Engines **Thrust Structure** Gimbals Avionics Wiring Reserve **Total Inert Mass** UNIVERSITY OF ARYLAND

12,240 kg 1245 kg 2482 kg 1626 kg 1905 kg 2236 kg

13,052 kg



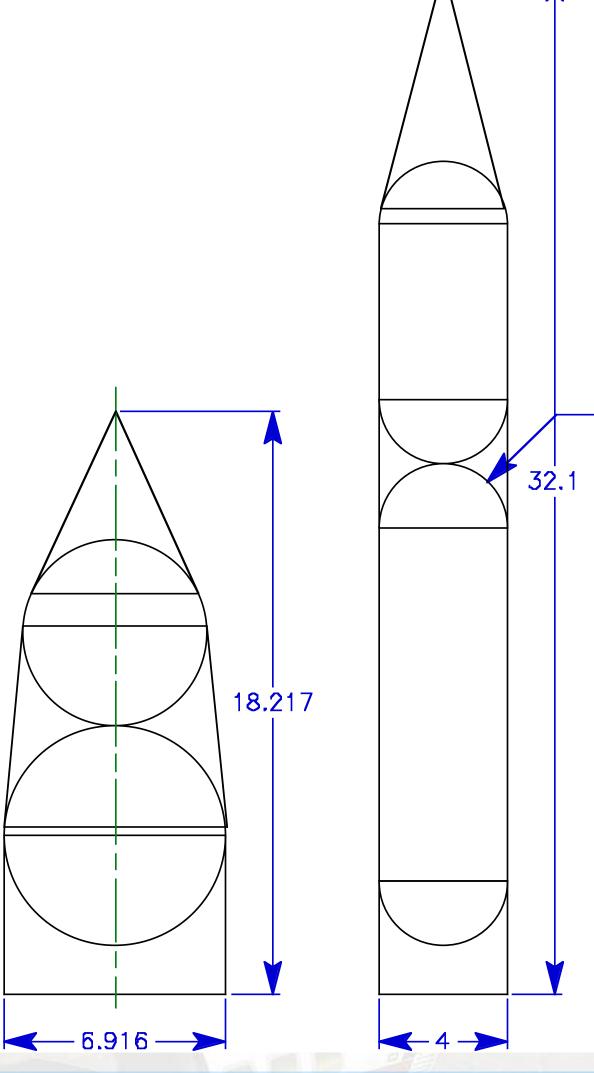
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Modifications for Second Pass

- Keep all initial vehicle sizing parameters constant
- Pick vehicle diameter and make tanks cylindrical to fit • Redo MER analysis

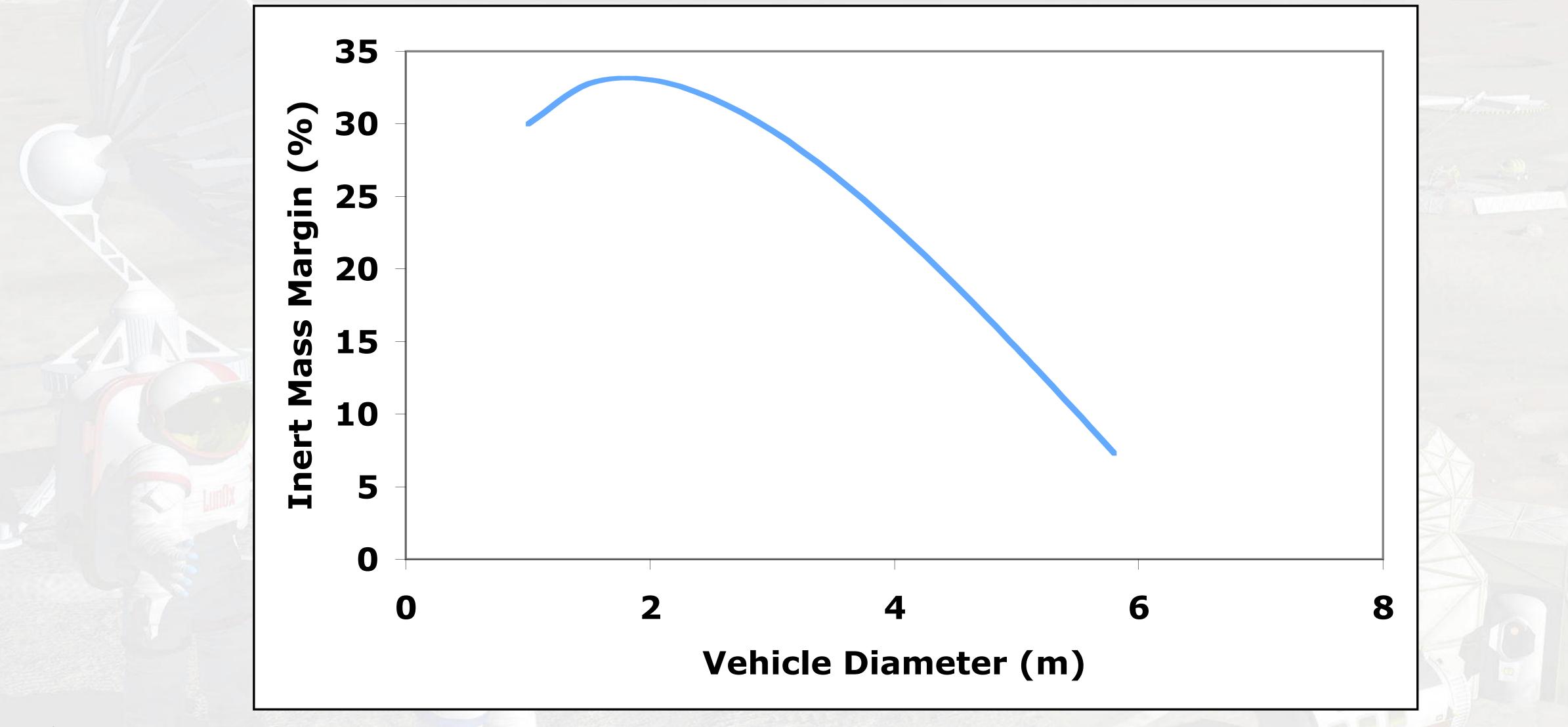








Effect of Vehicle Diameter on Mass Margin



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Effect of Mass-Optimal Diameter Choice

- Mass-optimal vehicle has diameter=1.814 m
- Mass margin goes from -6.22% to +33.1%
- Vehicle length=155 m
 - of spaghetti
- No volume for six rocket engines in aft fairing
- Infeasible configuration

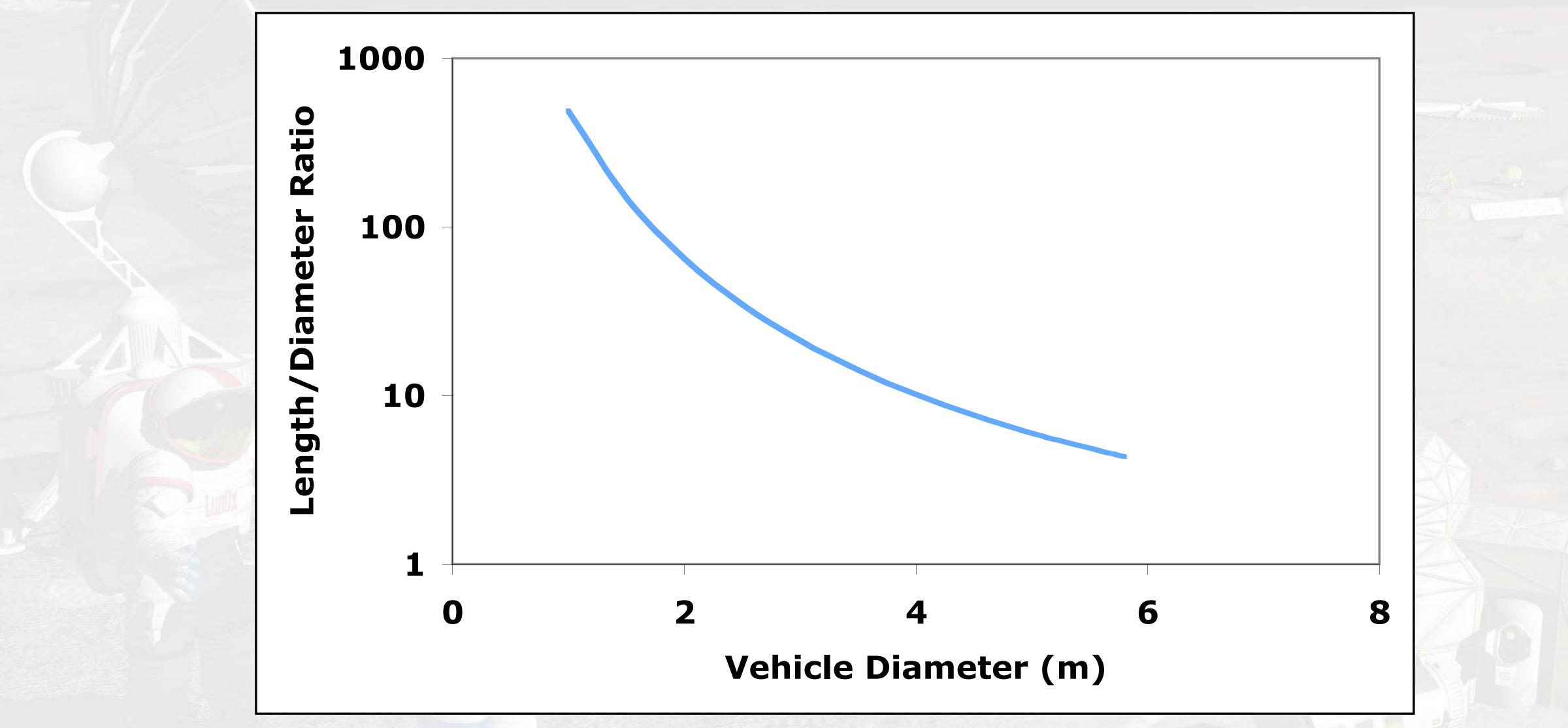


• Length/diameter ratio=86 – approximately equivalent to piece

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Effect of Diameter on Vehicle L/D

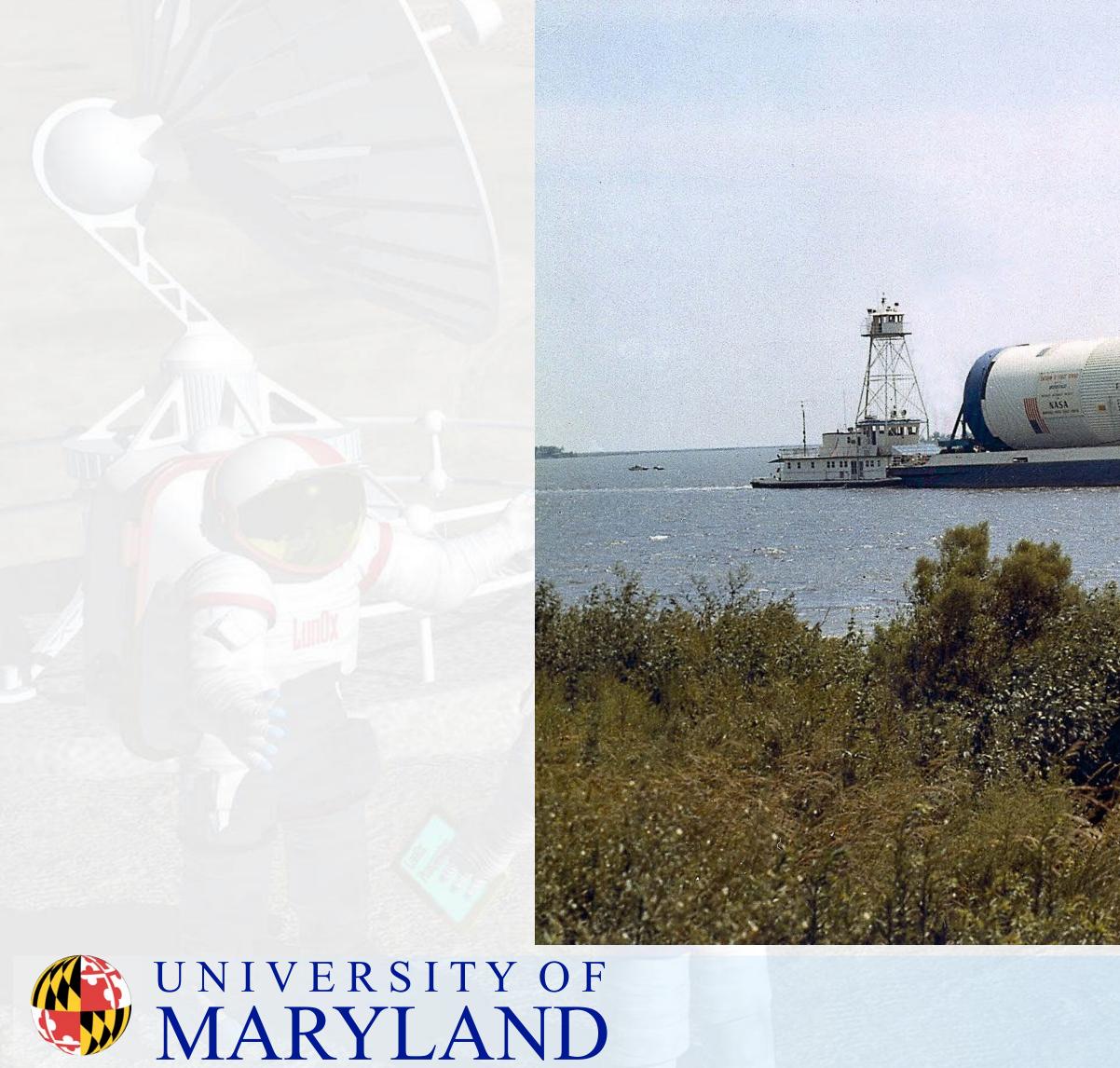


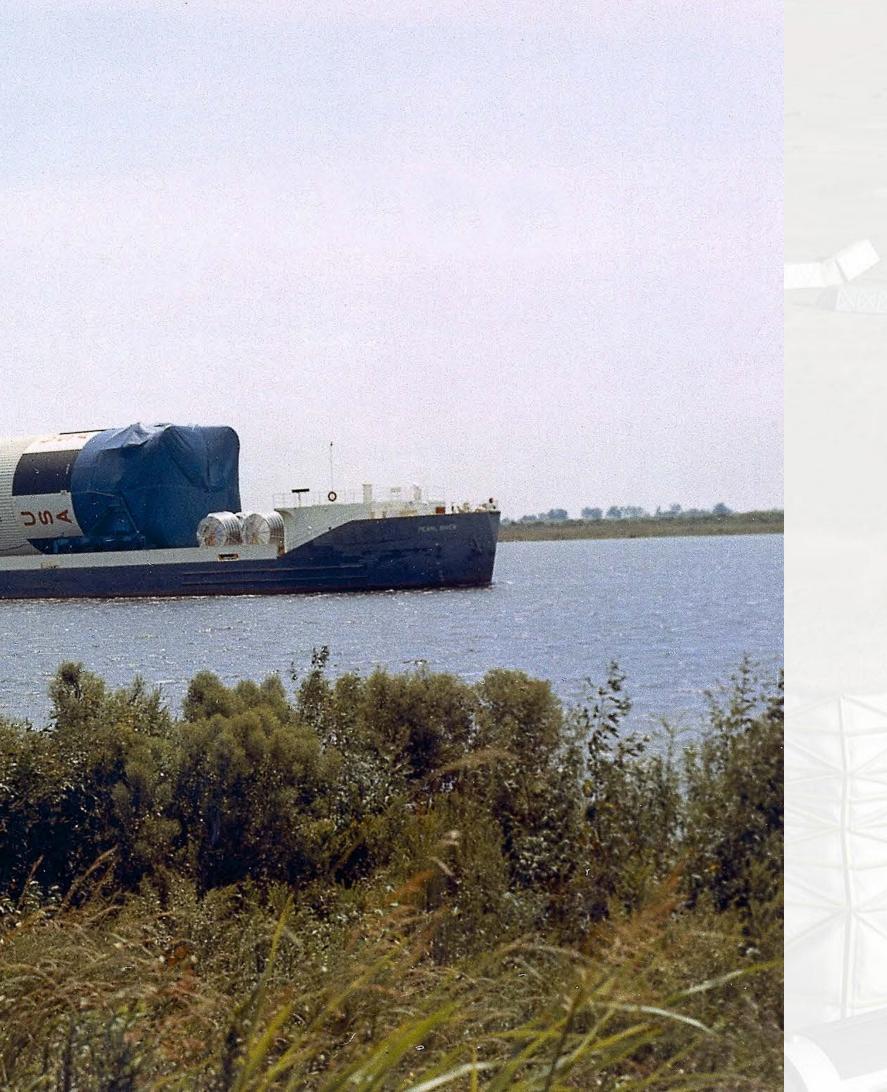
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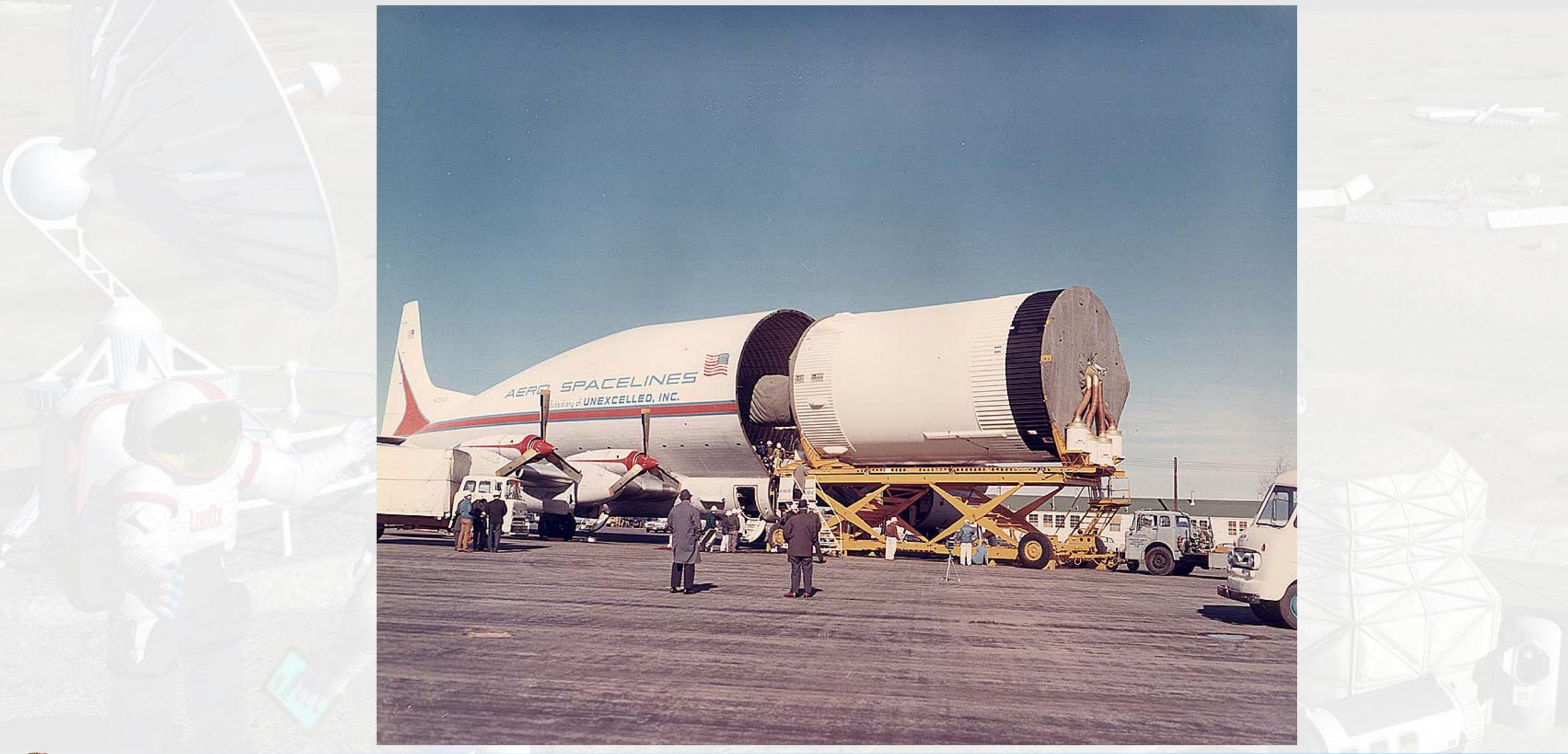
S-IC Barge Delivery (10m diameter)







S-IVB Air Transport (7m diameter)







Atlas/Delta Delivery System (4-5m diam)







SpaceX Falcon 9 Delivery (3.7m diam)



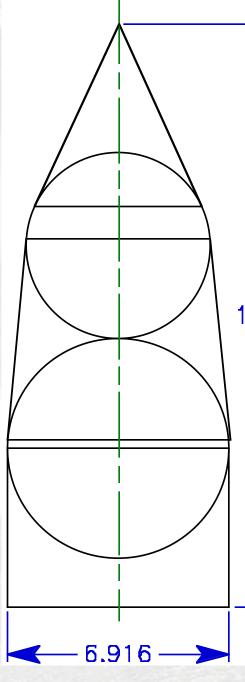
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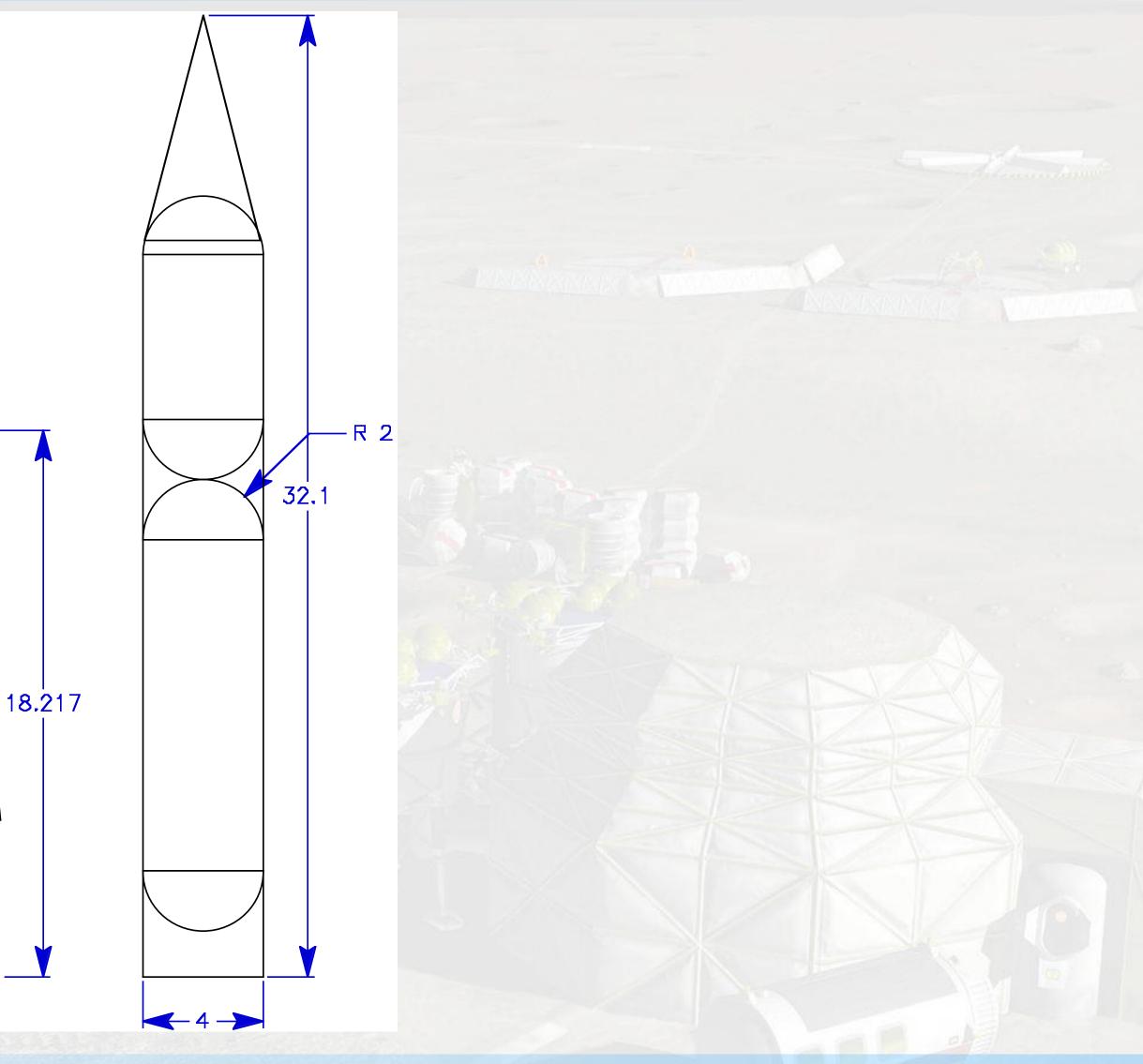


Second Pass Vehicle Configuration





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Mass Summary - Second Pass

Initial Inert Mass Estimate12,240 kg12,240 kg LOX Tank 1245 kg 1245 kg 2482 kg LH2 Tank 2482 kg LOX Insulation 119 kg 56 kg 145 kg LH2 Insulation 586 kg Payload Fairing 402 kg 645 kg **Intertank Fairing** 448 kg 1626 kg Aft Fairing 1905 kg 579 kg 2236 kg 2236 kg Engines **Thrust Structure** 497 kg 497 kg Gimbals 81 kg 81 kg 744 kg Avionics 744 kg 1044 kg Wiring 886 kg Reserve **Total Inert Mass** 13,052 kg 9960 kg UNIVERSITY OF ARYLAND

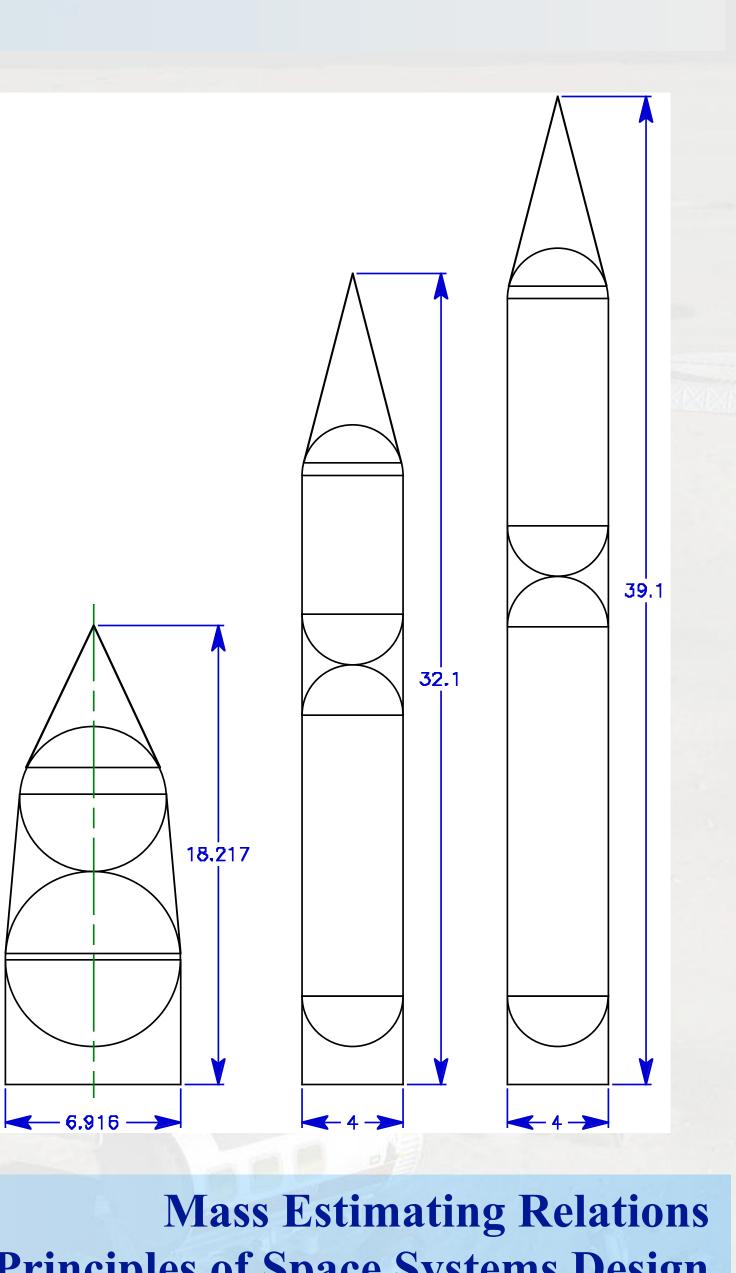
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Modifications for Iteration 3

• Keep 4 m tank diameter • Change initial assumption of δ iteratively, with resulting changes in m₀ and m_i, to reach 30% mass margin • Modify diameter to keep $L/D \le 10$ and iterate again for optimal initial mass estimate





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Vehicle-Level Prelim Design - 3rd Pass • Single Stage to Orbit (SSTO) vehicle • $\Delta V = 9200 \text{ m/sec}$ $r = e^{-\frac{\Delta V}{Ve}} = 0.1127$ 5000 kg payload $\lambda = r - \delta = 0.0294$ • LOX/LH2 propellants - Isp=430 sec $M_o = \frac{M_\ell}{\lambda} = 169,800 \ kg$ (Ve=4214 m/sec) $- \delta = 0.08323$ $M_i = \delta M_o = 14,130 \ kg$ • Diameter=4.2 m $M_p = M_o(1-r) = 150,700 \ kg$ • L/D=9.7 UNIVERSITY OF MARYLAND

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Mass Summary - Third Pass

Initial Inert Mass Estimate12,240 kg12,240 kg 14,130 kg 1245 kg 1382 kg 1245 kg LOX Tank LH2 Tank 2482 kg 2482 kg 2755 kg LOX Insulation 119 kg 56 kg 62 kg 586 kg 145 kg 160 kg LH2 Insulation 645 kg 402 kg 427 kg Payload Fairing Intertank Fairing 1626 kg 448 kg 501 kg 1905 kg 579 kg Aft Fairing 626 kg 2236 kg 2443 kg 2236 kg Engines **Thrust Structure** 497 kg 497 kg 552 kg Gimbals 81 kg 90 kg 81 kg 744 kg 744 kg 773 kg Avionics 886 kg 1044 kg 1101 kg Wiring Reserve 3,052 kg 9960 kg 10,870 kg -6.22 % +22.9 % +30.0 % **Total Inert Mass** 13,052 kg Design Margin UNIVERSITY OF MARYLAND **Mass Estimating Relations ENAE 483/788D – Principles of Space Systems Design** 45



Mass Budgeting

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Initial Inert Mass Estimate14,131 kg14,131 kg 1382 kg LOX Tank 2755 kg LH2 Tank LOX Insulation 62 kg 72 kg 160 kg LH2 Insulation 427 kg Payload Fairing Intertank Fairing 501 kg Aft Fairing 626 kg 2443 kg Engines 552 kg **Thrust Structure** Gimbals 90 kg 773 kg Avionics Wiring 1101 kg Reserve 10,870 kg 12,500 kg **Total Inert Mass** UNIVERSITY OF

Estimates Budgeted Margins 1589 kg 207 kg 3168 kg 413 kg 9 kg 184 kg 24 kg 491 kg 64 kg 576 kg 75 kg 720 kg 94 kg 2809 kg 366 kg 634 kg 83 kg 103 kg 13 kg 889 kg 116 kg 1267 kg 165 kg 1630 kg

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Masses of Pressurized Systems Spacecraft/Stations/Habitats • Gross mass

• Pressure hull mass

Internal systems mass





 $m_G < kg > = 460V < m^3 >^{0.76}$

$m_{hull} < kg >= 91.03V < m^3 >^{0.83}$

$m_{sys} < kg > = 366.3V < m^3 > 0.74$

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Today's Tools

- Heuristic equations for estimating mass of vehicles at a component level
- Concept of mass margin as a design driver • Budgeting of margin for future levels of design detail



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References

- C. R. Glatt, WAATS A Computer Program for Weights Analysis of Advanced Transportation Systems NASA CR-2420, September 1974. 1978.
- D-6349, May 1971
- Based on Historical Data NASA JSC-26098, November 1994

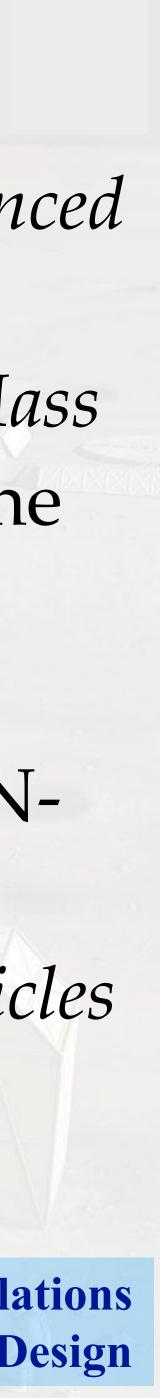


• I. O. MacConochie and P. J. Klich, Techniques for the Determination of Mass Properties of Earth-to-Orbit Transportation Systems NASA TM-78661, June

• Willie Heineman, Jr., Fundamental Techniques of Weight Estimating and Forecasting for Advanced Manned Spacecraft and Space Stations NASA TN-

• Willie Heineman, Jr., Mass Estimation and Forecasting for Aerospace Vehicles

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2024 Project Themes

- Long-Duration Mars Simulation at the Moon (RASC-AL) Sustained Lunar Evolution (RASC-AL) Large-Scale Lunar Crater Prospector (RASCAL)
- Collaborative Robotic Lunar Rovers (GSFC)





Long-Duration Mars Simulation at the Moon

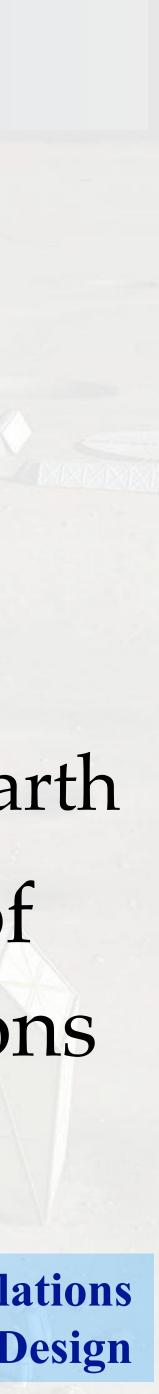
• Develop an architecture for a long-duration simulation of a Mars mission conducted at the Moon, e.g.

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delays representing a Mars transit hub starting NLT 2035 – Land on the Moon and perform a 30-day exploration mission



- 12-month microgravity stay in cislunar space with artificial comm
- Return to cislunar habitat and stay for 12 months before return to Earth
- Focus on habitats and transit vehicles to maximize fidelity of the Mars mission simulation; safety systems and abort options



Sustained Lunar Exploration Infrastructure

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• Develop an architecture for evolving human presence on the Moon to expand available services and commodities consumables), power, comm, navigation, and cargo transport – Initially for south polar region but expandable to rest of Moon costs charged to users to make it economically viable global support capabilities



- Service architecture should provide logistics (propellant and crew

– Design systems and operations as commercial endeavor, including

– South polar services available NLT 2035, provide growth plans to



Large-Scale Lunar Prospector

- long durations in craters at the lunar south pole - Should be capable of determining location, composition, and regions

 - Describe concept of operations, configuration and subsystems, integration into rovers and transports
 - Ready for initial operations NLT 2033 UNIVERSITY OF MARYLAND

• Develop a concept for a prospecting rover that can operate for

accessibility of water ice and other volatiles in permanently shadowed

- Capable of operating within the crater for up to a year with extended sorties into PSRs – focus on designing for extreme cold and darkness

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Collaborative Lunar Exploration Rovers (GSFC)

- Exploration of lunar permanently shadowed regions by a network of cooperative instruments
 - Interactive design process with NASA Goddard scientists advising on science goals and instrument details - Spatial and temporal measurements of volatiles in PSRs - Measurement of regolith properties to understand weathering in PSRs Option for astronaut involvement in operations - Hardware demonstrations using smaller hobby-level robotic hardware?





Matrix Organization

ENAE484

 Systems Analysis/Systems Engineering (SASE) – Mission Planning and Analysis (MPA) – Loads, Structures, and Mechanisms (LSM) – Power, Propulsion, and Thermal (PPT) – Crew Systems (CS) – Avionics, Flight Software, and Simulations (AFSS)

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• Each project team will be divided into six specialty groups for





Systems Analysis/Systems Engineering

- Mission architecture
- Systems engineering
- Vehicle- and system-level trade studies

- Cost estimation
- Risk analysis / tracking
- Tracking of vehicle center of gravity and inertia matrix
- Advanced technology (e.g., robotics, EVA)

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• Creation and tracking of budgets, particularly mass and cost Maintenance of canonical system configuration documents

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Mission Planning and Analysis

- Creation and maintenance of design reference mission(s) (DRM)

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- Orbital mechanics and launch/entry trajectories Determination of operational mission objectives Concept of operations (CONOPS)
- Programmatic planning (sequence of missions)
- Science instrument/payload definition





Loads, Structures, and Mechanisms

- Identification and estimation of loads sources
- Structural design and analysis
 - Selection of structural shapes and materials
 - Stress modeling
 - Deformation estimation
 - Design optimization
- Design of mechanisms (e.g., docking/berthing ports,
- Tracking of critical margins of safety UNIVERSITY OF MARYLAND

separation mechanisms, launch hold-downs, engine gimbals))



Power, Propulsion, and Thermal

- Electrical power generation
- Energy storage
- Power management and conditioning
- Primary propulsion (orbital maneuvering)
- Reaction control system (rotation / translation)
- Design of propellant storage and feed systems
- Thermal modeling and analysis
- Thermal control systems
- Power budgets

UNIVERSITY OF MARYLAND nditioning maneuvering) ation/translation) e and feed systems ysis



Crew Systems

- Internal layout
- Emergency egress systems
- Lighting and acoustics
- Window and viewing analysis
- Life support systems
 - Air revitalization
 - Water collection and regeneration
 - Cabin thermal control
 - Waste management
 - Food and hygiene
- EVA accommodations UNIVERSITY OF MARYLAND



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Avionics, Flight Software, and Simulation

- Data management (flight computers)
- Networking
- Sensors
- Power distribution
- Guidance system
- Control systems, including attitude control
- Communications
- Robot control systems
- Software
- Data transmission budgets
- Simulations UNIVERSITY OF

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Selecting Assignments for 484

- ignore this slide
 - linked survey form
- Pairwise comparisons for term project
- Pairwise comparisons for specialty assignment
- Check on schedule conflicts
- I will go through an AHP process and then sort you into groups and specialties

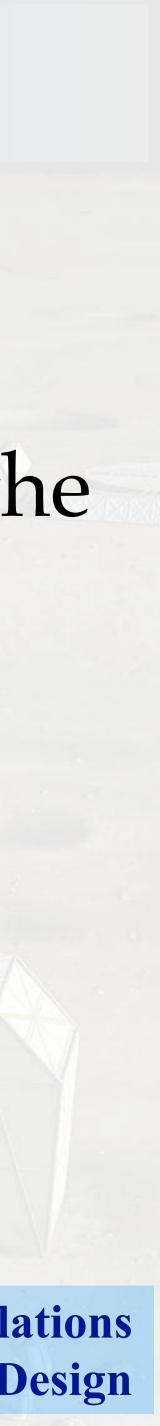




• If you are a grad student or not taking ENAE 484 next term,

• Go to the course site on spacecraft.ssl.umd.edu and fill out the

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In-Class Prompt

- Divide up into groups of 6-8 and discuss 484 projects and specialties • If you have any questions, I'll be wandering around to answer them
- If you are grad students or hypersonic capstone students, meet football games this season soon on the 483 splash page



in your own groups and discuss if we will win any more

• Look for the link to the selection survey which will be posted

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