

Robotic Mobility – Atmospheric Flight

- Gaseous planetary environments (Mars, Venus, Titan)
- Lighter-than-“air” (balloons, dirigibles)
- Heavier-than-“air” (aircraft, rotorcraft)



Exponential Atmospheres

$$\rho = \rho_o e^{-h/h_s}$$

ρ_o = Reference density

h_s = Scale height



Atmospheric Density with Altitude

Pressure=the integral of the atmospheric density in the column above the reference area

$$\rho = f(h) \quad P_o = \int_0^\infty \rho g dh = \rho_o g \int_0^\infty e^{-\frac{h}{h_s}} dh = -\rho_o g h_s \left[e^{-\frac{h}{h_s}} \right]_0^\infty \\ = -\rho_o g h_s [0 - 1]$$

$$P_o = \rho_o g h_s$$

$$\text{Earth: } \rho_o = 1.226 \frac{\text{kg}}{\text{m}^3}; h_s = 7524\text{m};$$

$$P_o(\text{calc}) = 90,400 \text{ Pa}; P_o(\text{act}) = 101,300 \text{ Pa}$$

ρ_o, P_o

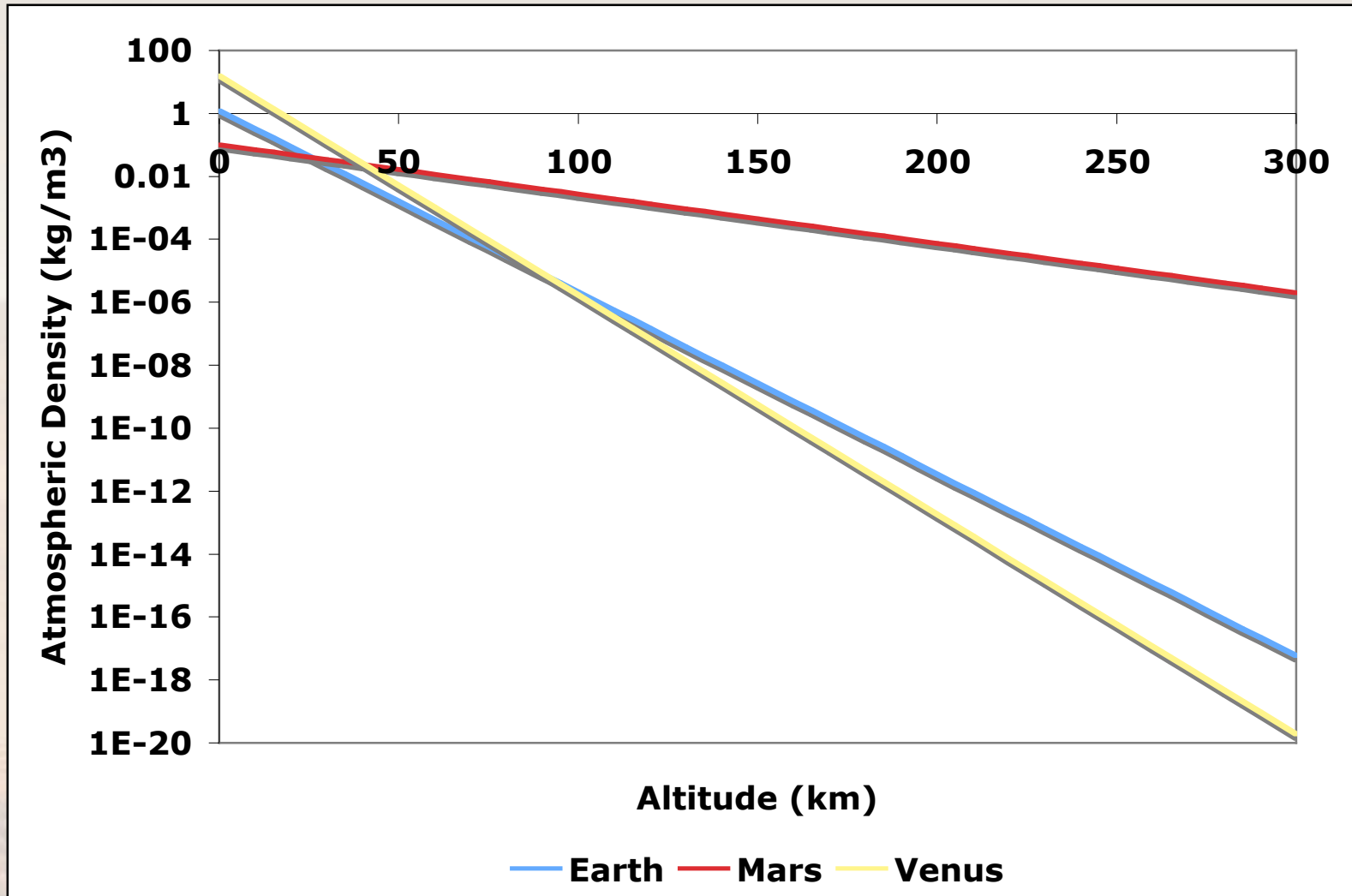


Planetary Entry - Physical Data

	Radius (km)	μ (km)	ρ_o (kg/m	h (km)	v (km/sec)
Earth	6378	398,604	1.225	7.524	11.18
Mars	3393	42,840	0.0993	27.7	5.025
Venus	6052	325,600	16.02	6.227	10.37
Titan			5.474	23.93	



Comparison of Planetary Atmospheres



Atmospheric Neutral Buoyancy

- Given an enclosed volume V of gas with density ρ
- Lift force is $V(\rho_{\text{atm}} - \rho)$ - must be $\geq mg$
 - on Earth ~ 1 kg lift / cubic meter of He
 - on Mars ~ 10 gms lift / cubic meter of He
- Horizontal velocity at equilibrium is identical to wind speed
- Interior pressure generally identical to ambient (except for superpressure balloons)
- Can generate low density through choice of gas, heating



Buoyancy by Light Gases

- Ideal gas law $PV = nRT$
- Given same volume and temperature, gas densities scale proportionally to molecular weight n
- Mars' atmosphere is essentially CO_2 – $n = 44$
 - He: $n = 4; \Delta \quad \rho = 90.3 \text{ gm}/\text{m}^3$
 - H_2 : $n = 2; \Delta \quad \rho = 94.8 \text{ gm}/\text{m}^3$
- *Hindenburg* airship would have a total lift capacity of 49,894 kg in Mars atmosphere and gravity (Earth lift capacity 232,000 kg - factor of 4.6)



Thermal Balloons (“Montgolfieres”)

- Use ambient gases and thermal difference to create lift
- Ideal gas – gas density inversely proportional to temperature
- Ambient atmospheric temperature on Mars ~200K
- Heat gases to 300K: lift force 33 gm/m³ (about 1/3 of He or H₂ balloon)



Superpressure Balloons

- Interior pressure greater than external ambient
- Envelope is relatively insensitive (in terms of volume) to interior pressure changes
- Diurnal temperature changes have minimal effect on lift
- Provides stable long-term platform for extended flights
- Envelope must be significantly stronger (and therefore heavier) than ambient-pressure balloons

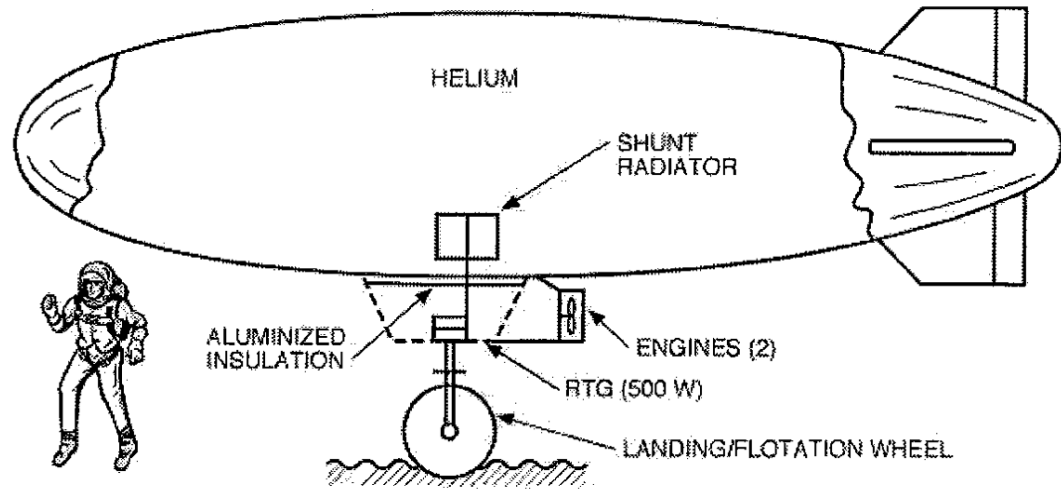
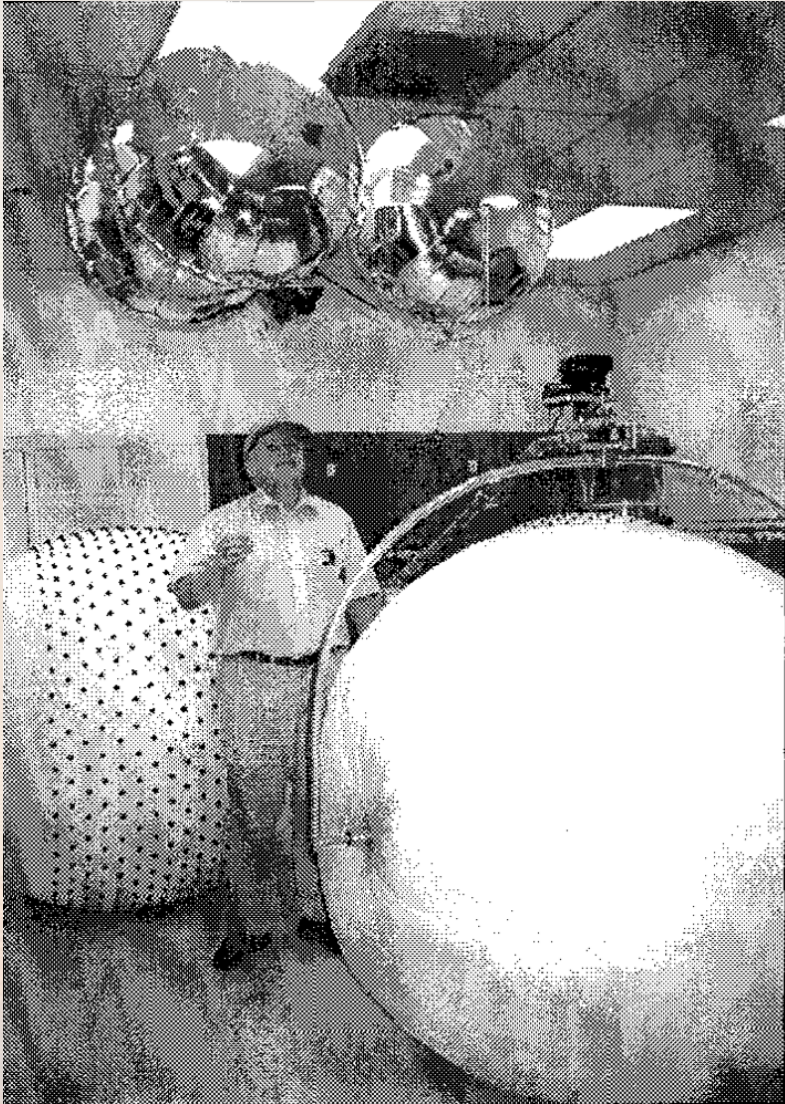


Flight Missions with Balloons

- Venus: Vega - Russian Vega missions put two French balloons in Venus atmosphere in 1985
 - One died in 56 minutes
 - One operated for two days (battery limitations)
- Mars: French dual-balloon system (solar thermal balloon tied to He/H₂ balloon - gas balloon keeps solar balloon off the ground, thermal balloon lifts payloads when sun warms envelope) -never flew



Future Concepts – Titan Aerover



UNIVERSITY OF
MARYLAND

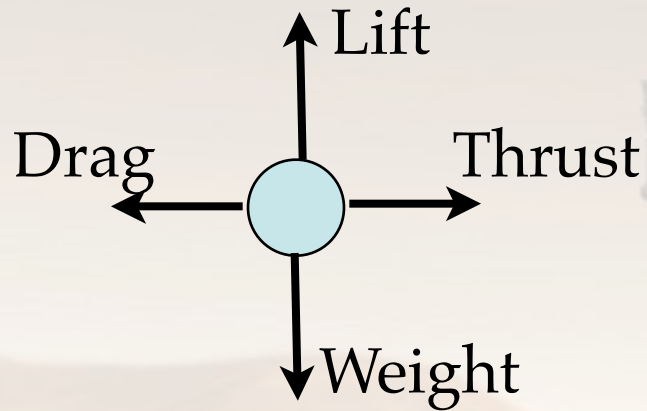
Robotic Mobility – Above the Surface
ENAE 788X - Planetary Surface Robotics

“Heavier than Atmosphere” Approaches

- Fixed wing
 - Gliders
 - Powered
 - Propellers
 - Jet
 - Rocket
- Rotary wing
- Hybrid / Reconfigurable



Dynamic Atmospheric Lift



$$D = \frac{1}{2} \rho v^2 S C_D$$

$$L = \frac{1}{2} \rho v^2 S C_L$$

For steady, level flight: $T = D$ $L = W = mg$

$$W = L = D \frac{L}{D} = T \frac{L}{D} \qquad T = \frac{W}{L/D}$$

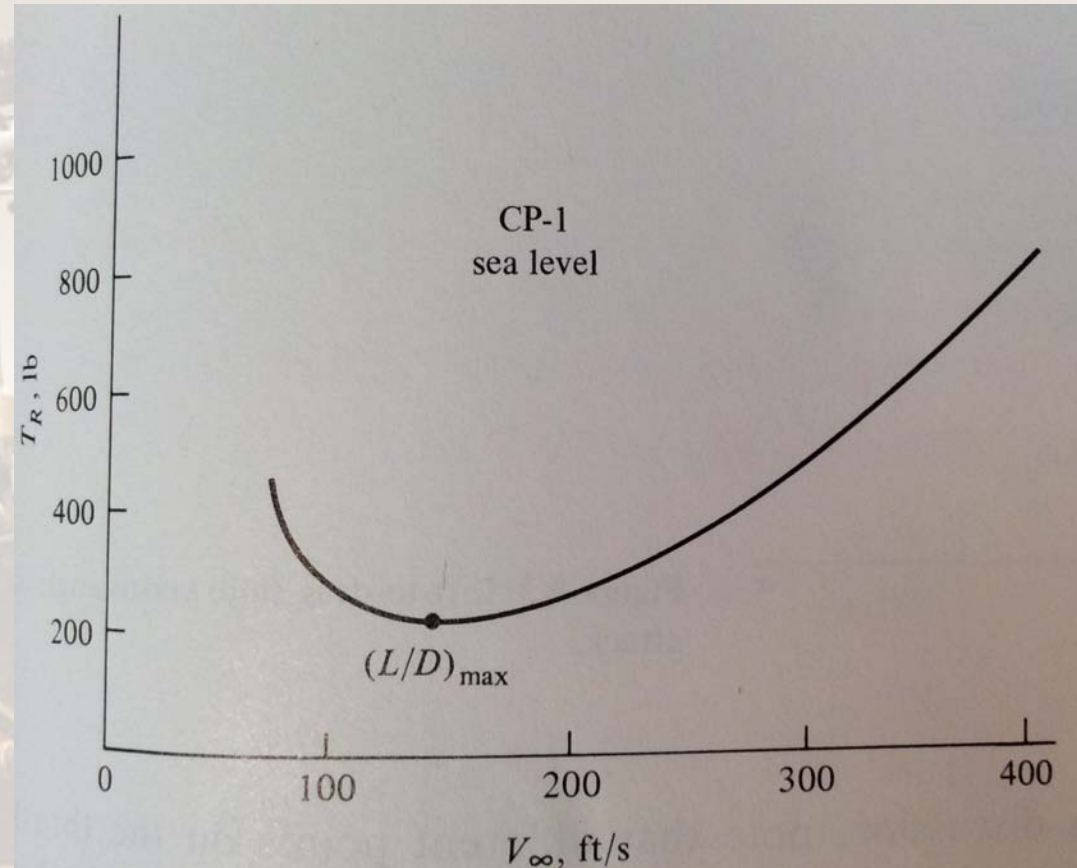
$$L = \frac{1}{2} \rho v^2 S C_D \frac{L}{D}$$



Atmospheric Flight Performance

$$L = \frac{1}{2} \rho v^2 S c_L$$

$$D = \frac{1}{2} \rho v^2 S c_D$$

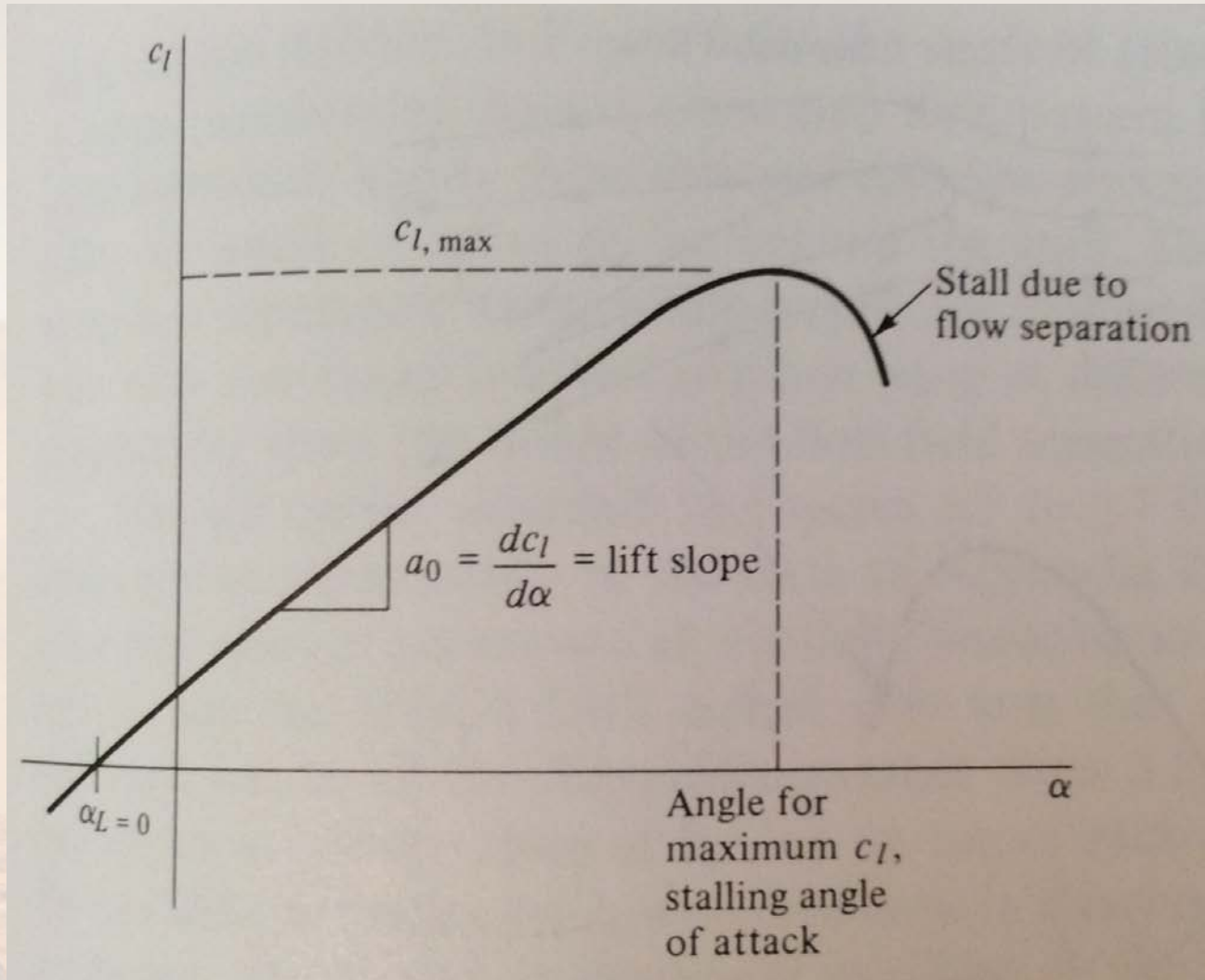


from Anderson, *Introduction to Flight*, Third Edition McGraw Hill, 1989

$$c_D = c_{D_o} + c_{D_i} = c_{D_o} + \frac{c_L^2}{\pi e (AR)}$$



Lift Curve



from Anderson, *Introduction to Flight*, Third Edition McGraw Hill, 1989



Mars Atmosphere

$$\rho = 0.020 \frac{\text{kg}}{\text{m}^3}$$

$$T = 210 \text{ K}$$

$$g = 3.71 \frac{\text{m}}{\text{sec}^2}$$

$$R = 188.92 \frac{\text{J}}{\text{kg K}}$$

$$\gamma = 1.2941$$

$$\text{Speed of sound } a = \sqrt{\gamma RT} = 226.6 \frac{\text{m}}{\text{sec}}$$



Aircraft Flight Performance



- U-2 high-altitude spy plane
- Cruises at “70,000+ feet”
- $m=18,000$ kg
- $b=32$ m
- $S\sim 64$ m²

$$v_{stall} = \sqrt{\frac{mg}{S} \frac{2}{\rho C_{L(max)}}}$$

$$\text{U-2 } v_{stall(Mars)} = 228.4 \frac{m}{sec^2}$$



Stable Gliding Flight

Flight path angle γ

$$D = mg \sin \gamma$$

$$mg = W = L \implies \sin \gamma = \frac{1}{L/D}$$

High performance glider $L/D \approx 30$

Deploy at 10 km \implies Range ≈ 300 km

$V \approx 200 \frac{m}{sec} \implies$ Flight time 25 min



Powered Flight

$$T = \dot{m}(v_e - V)$$

v_e = Exhaust velocity; V = Flight velocity

$$\text{Power into flow } P_f = \frac{\dot{m}}{2} (v_e^2 - V^2)$$

$$\text{Power into flight } P_v = TV$$

$$\text{Propulsive efficiency } \eta_{prop} = \frac{2}{1 + \frac{v_e}{V}}$$



Actuator Disk Size

Engine intake area A

$$\dot{m} = \rho AV \qquad T = D = \frac{W}{L/D}$$

$$T = \dot{m}V = \rho AV(v_e - V)$$

$$\rho AV(v_e - V) = \frac{W}{L/D}$$

$$A = \frac{W}{(L/D)\rho V(v_e - V)}$$



Rotorcraft (Quick and Dirty)

- Thrust is downwards
- Hovering flight $T=W$
- Power calculations same as before if $L/D=1$
- Incline lift vector angle β from vertical

$$W = T \cos \beta \implies T = \frac{mg}{\cos \beta}$$

$$D = T \sin \beta \implies D = mg \tan \beta$$

$$\frac{1}{2} \rho V^2 S c_D = mg \tan \beta \implies V = \sqrt{\frac{2mg \tan \beta}{\rho S c_D}}$$



Looking for Equation for Range

$$\text{Efficiency} = \frac{\text{propulsive power}}{\text{fuel power}} = \frac{T v_e}{\dot{m}_f h}$$

$$\eta_{\text{overall}} = \frac{T v_e}{\dot{m}_f h} \quad \frac{dW}{dt} = -\dot{m}_f g = \frac{-W}{\frac{L}{D} \frac{T}{\dot{m}_f g}}$$

$$\frac{dW}{dt} = \frac{-W v_e}{\frac{h}{g} \frac{L}{D} \frac{T v_e}{\dot{m}_f h}} = \frac{-W v_e}{\frac{h}{g} \frac{L}{D} \eta_{\text{overall}}}$$

