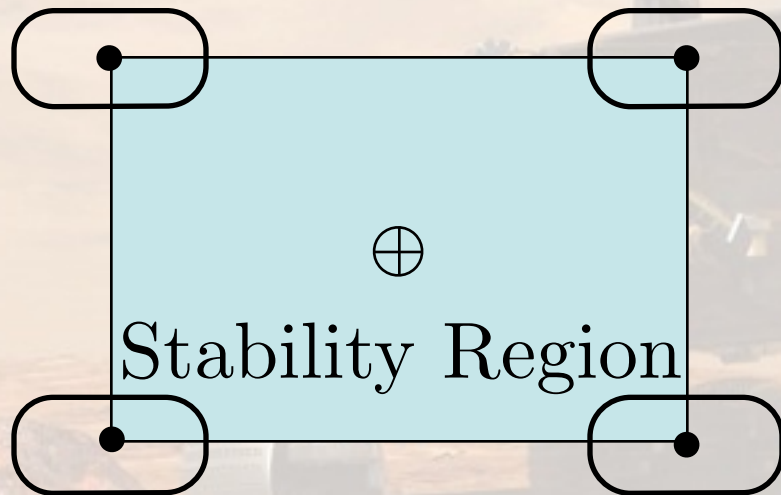
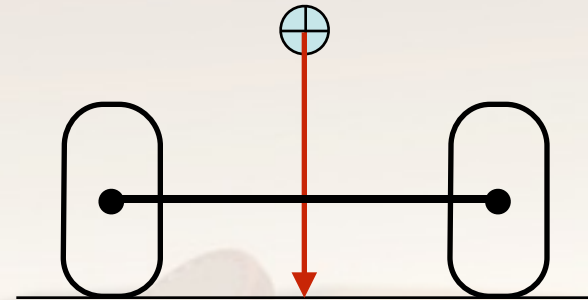
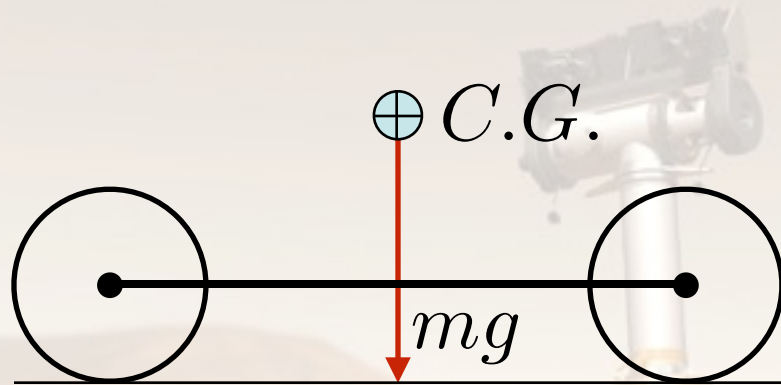


Slopes and Static Stability

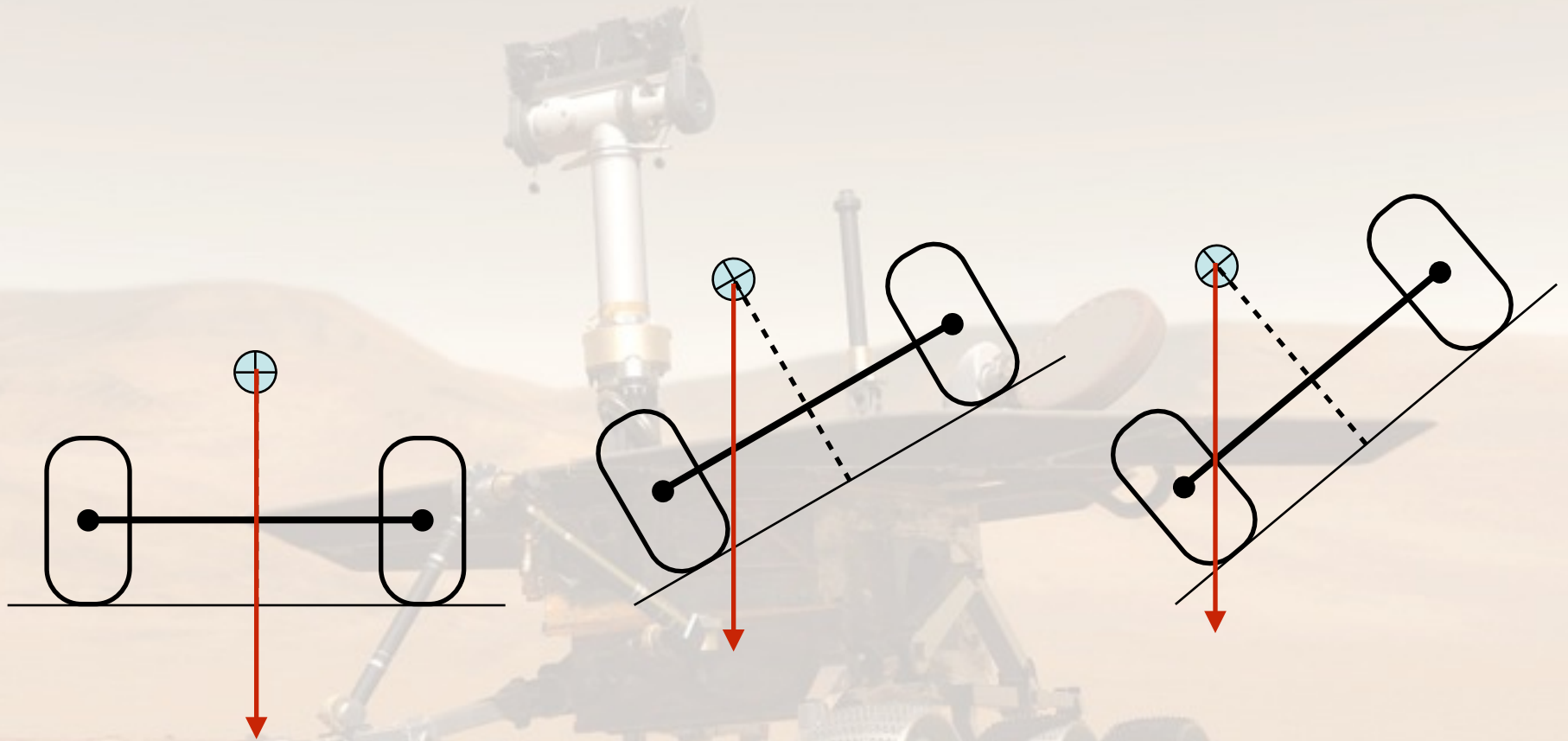
- Stability across and along slopes
- Forces and torques on wheels
- Acceleration/deceleration
- Turning
- Hitting obstacles
- Rigid suspensions and obstacles



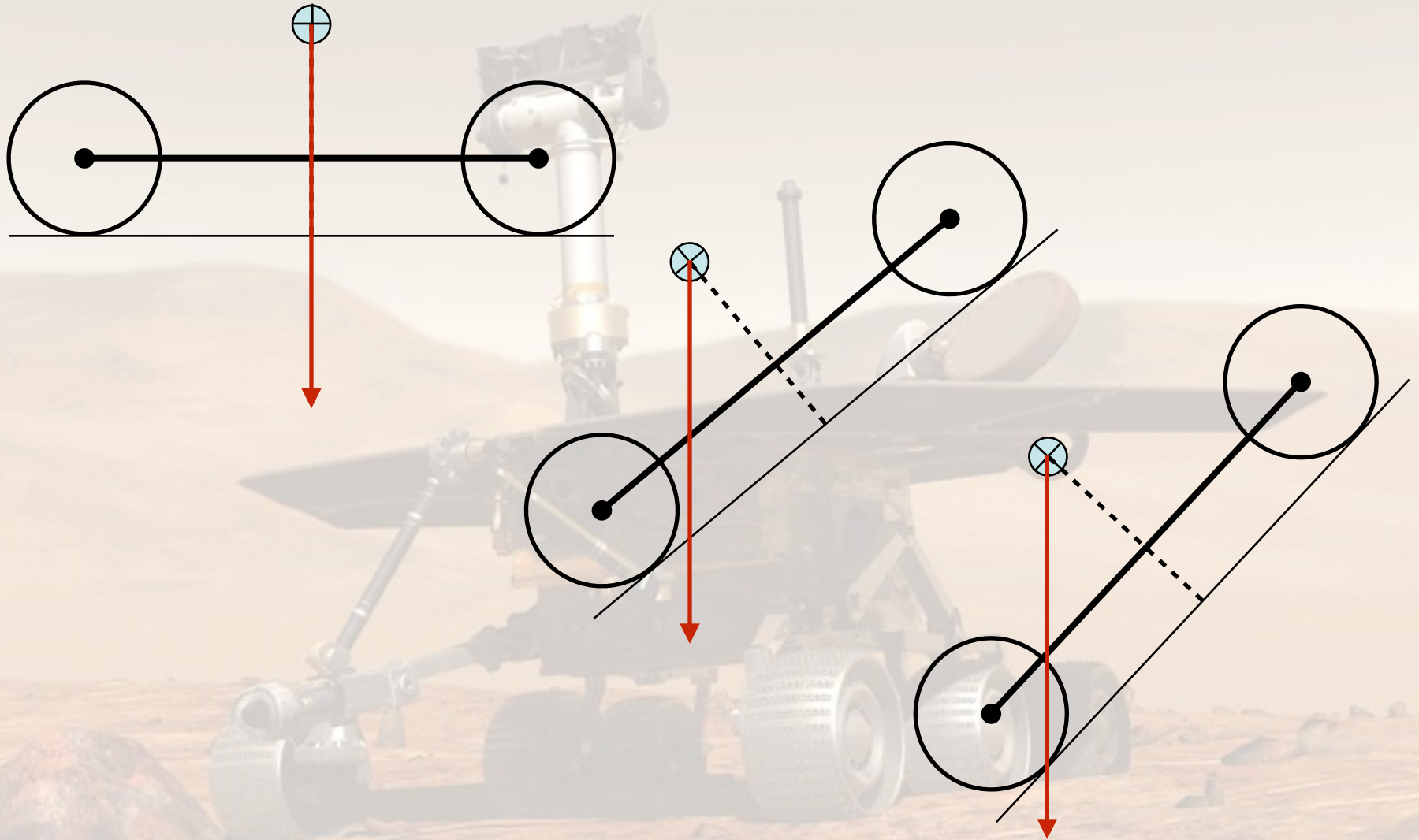
Rover with CG and Force Vector



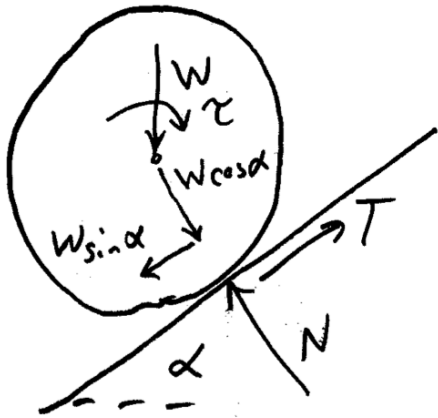
Rover on Cross Slope



Rover Climbing/Descending Slope



Slopes + Obstacles



Wheel coefficient of friction
with ground = μ

$N \equiv$ normal force to surface

$$\tau = \mu r N = \mu r W \sin \alpha$$

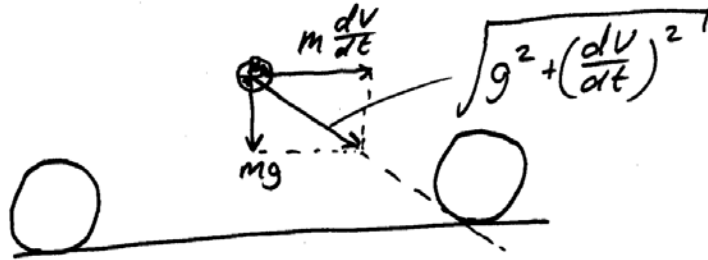
$$T = \mu N = \frac{\tau}{r} = W \sin \alpha$$

$$\mu W \cos \alpha = W \sin \alpha$$

$$\tan \alpha = \mu$$

Assume $\tau > \mu_{\text{limit}} N r$ (friction limited,
not torque limited)

Acceleration / Deceleration



Accel: "0-60 mph in _____ seconds"

$$60 \text{ mph} = 88 \text{ ft/sec} = 26.8 \text{ m/sec}$$

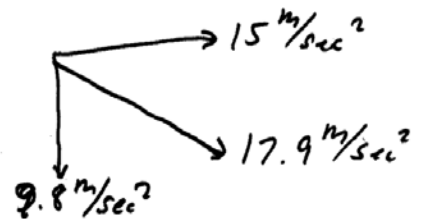
| Time (sec) | dV/dt (m/sec ²) | Earth accel total (g's) |
|------------|-------------------------------|-------------------------|
| 7 | 3.83 | 1.07 |
| 6 | 4.47 | 1.10 |
| 5 | 5.36 | 1.14 |
| 4 | 6.70 | 1.21 |

Decel: "1 car length / 10 mph"

60 mph, $l = 4 \text{ m} \Rightarrow 24 \text{ m}$ to stop

$$s = \frac{1}{2} at^2 \quad v = at \Rightarrow s = \frac{1}{2} \frac{v^2}{a} \quad a = \frac{1}{2} \frac{v^2}{s}$$

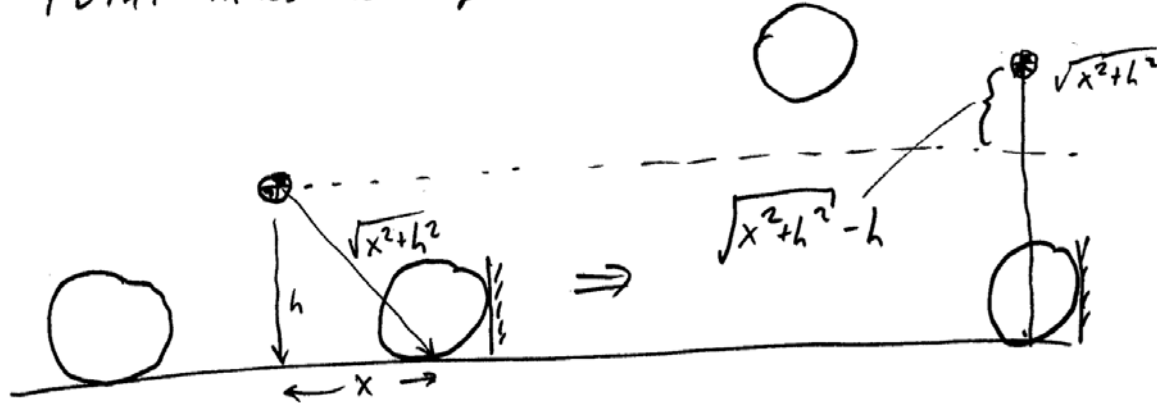
$$a_{\text{decel}} = \frac{(26.8 \text{ m/sec})^2}{2(24 \text{ m})} = 14.96 \text{ m/sec}^2$$



$$a_{\text{decel}} = 1.84 \text{ g}$$

Impulsive Pitchover Criteria

Point mass assumption \Rightarrow conservative estimate



$$KE = PE$$

$$mg(\sqrt{x^2 + h^2} - h) = \frac{1}{2} m V^2$$

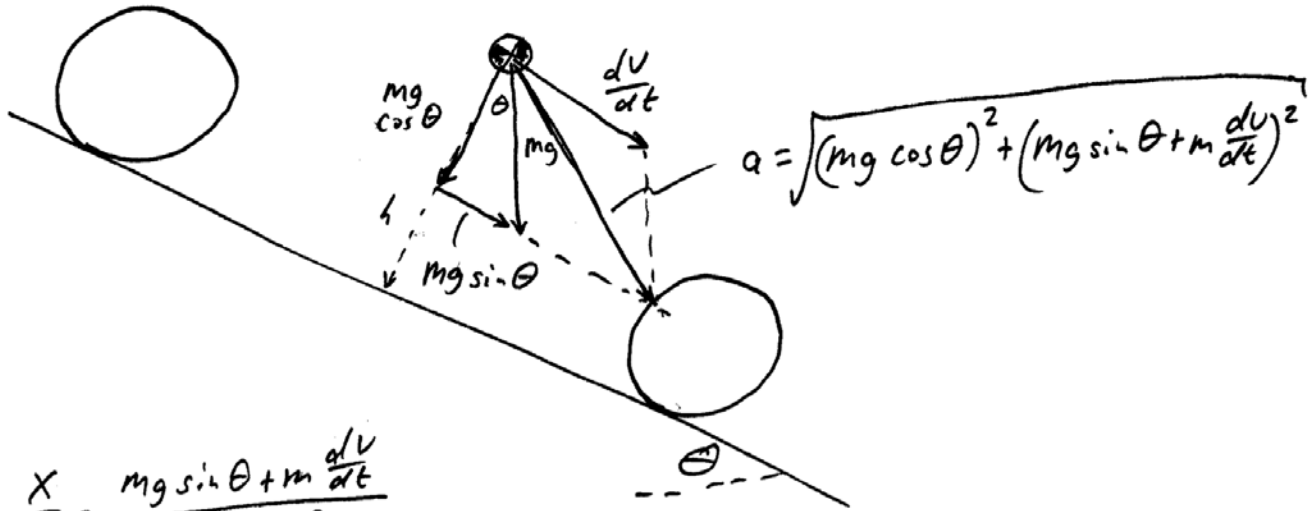
$$\sqrt{x^2 + h^2} = \frac{V^2}{2g} + h$$

$$\text{Moon: } \frac{x}{h} \Big|_{\text{crit}} = 1.969$$

$$x^2 + h^2 = \left[\frac{V^2}{2g} + h \right]^2$$

$$\frac{x}{h} = \sqrt{\frac{1}{h^2} \left[\frac{V^2}{2g} + h \right]^2 - 1} = \sqrt{\frac{V^2}{2gh} \left(\frac{V^2}{2gh} + 2 \right)}$$

Accel / Decel on Slopes



$$\frac{X}{h} = \frac{mg \sin \theta + m \frac{dV}{dt}}{mg \cos \theta}$$

$$= \frac{g \sin \theta + \frac{dV}{dt}}{g \cos \theta}$$

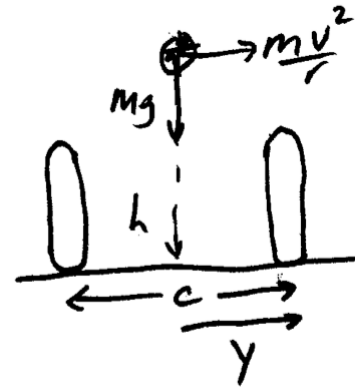
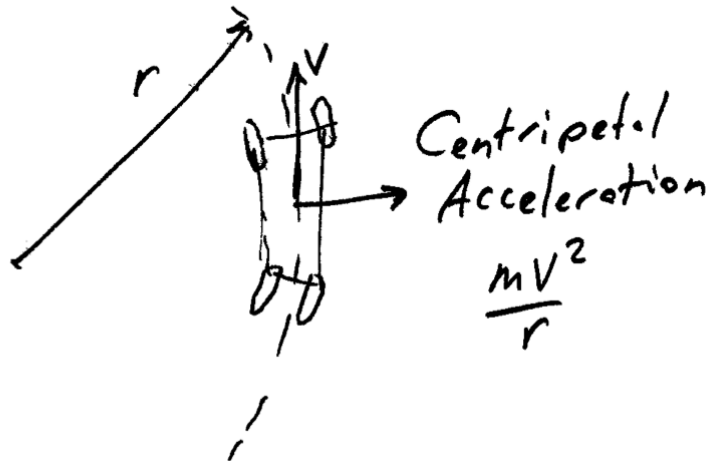
$$\text{if } \theta = 0 \Rightarrow \frac{X}{h} = \frac{\frac{dV}{dt}}{g} \quad \checkmark$$

$$\frac{X}{h} g \cos \theta = g \sin \theta + \frac{dV}{dt} \Rightarrow \frac{dV}{dt} = g \left(\frac{X}{h} \cos \theta - \sin \theta \right)$$

Moon: $\frac{X}{h} = 1$

| $\frac{dV}{dt} / \text{limit}$ | θ | $S_{\text{strip}} (10 \text{ km/hr})$ |
|--------------------------------|------------|---------------------------------------|
| 1.6 m/sec^2 | 0 | 2.42 m |
| 1.3 m/sec^2 | 10° | 3.0 m |
| 0.96 m/sec^2 | 20° | 4.0 m |
| 0.59 m/sec^2 | 30° | 6.5 m |

Lateral Stability



$$\frac{\gamma}{h} = \frac{m \frac{V^2}{r}}{mg} = \frac{V^2}{gr}$$

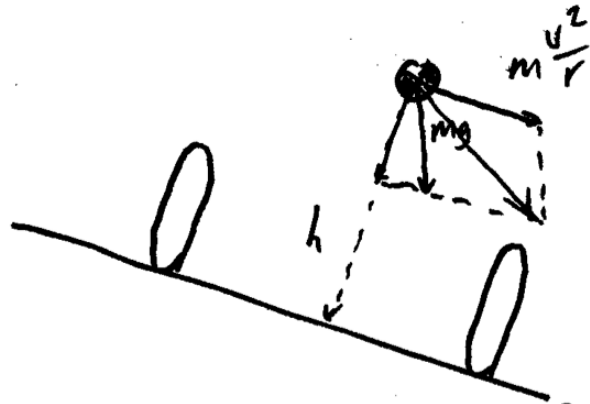
$$\text{set } \frac{\gamma}{h}, g \Rightarrow \frac{V^2}{r} = \text{constant} (= g \frac{\gamma}{h})$$

Doubling $V \Rightarrow$ increases $r \times 4$!!

$$r \propto \frac{1}{g} \text{ at same velocity}$$



Turning on a slope



$$\frac{Y}{h} = \frac{mg \sin \theta + m \frac{v^2}{r}}{mg \cos \theta}$$

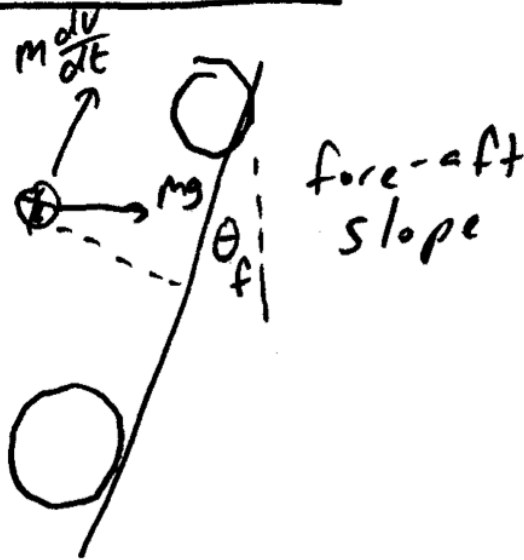
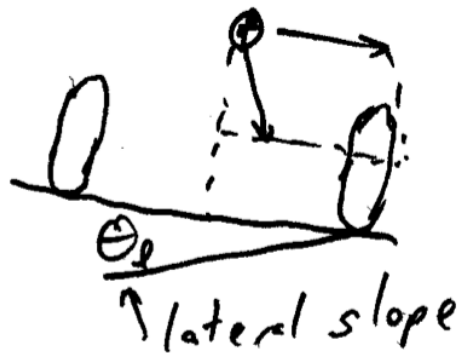
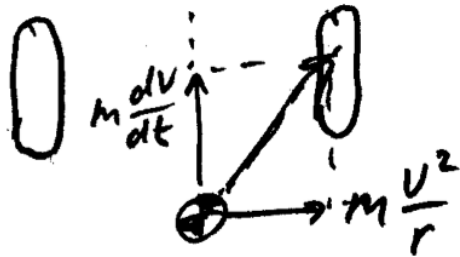
$$= \frac{\sin \theta + \frac{v^2}{gr}}{\cos \theta}$$

$$\frac{Y}{h} \cos \theta - \sin \theta = \frac{v^2}{gr}$$

$$r = \frac{v^2}{g} \left[\frac{Y}{h} \cos \theta - \sin \theta \right]^{-1}$$



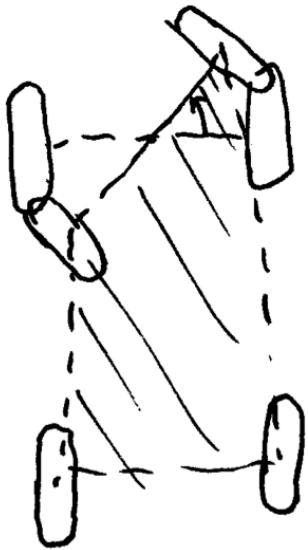
Composite Stability



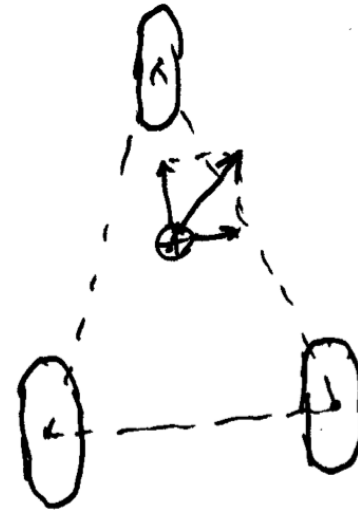
For conventional configuration,
 (rectangular stability region)
 lateral and longitudinal
 stability are decoupled



Alternative Configurations



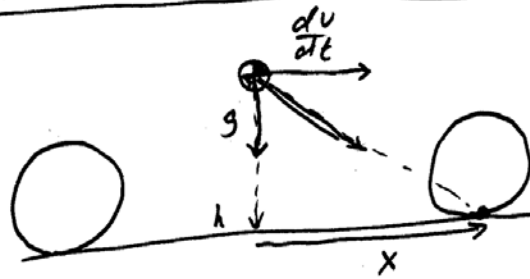
Wagon Steering



Lateral and longitudinal forces are stable alone, but unstable together.



Deceleration Stability Limits



$$\frac{x}{h} = \frac{dV/dt}{g}$$

| | $V=60\text{mph}$ $dV/dt=15\text{m/sec}^2$ $(x/h)\text{ limit}$ | $V=10\text{mph}$ $dV/dt=2.5\text{m/sec}^2$ |
|-------|--|---|
| Earth | 1.53 | 0.255 |
| Mars | 4.03 | 0.658 |
| Moon | 9.38 | 1.56 |

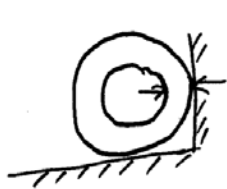
Less stable in lower gravity

60 mph panic stop on Earth = 10 mph panic stop on Moon

for given $\frac{x}{h}$: $\left. \frac{dV}{dt} \right|_{\text{limit}} \propto g$ $S_{\text{min}} \propto \frac{1}{g}$

60 mph panic stop on Moon requires 147 m !!

"Hitting a Wall"



$S_{\text{stop}} \sim \text{tire thickness}$
 $\sim 0.3 \text{ m}$

e.g., pressurized rover @ 4000 kg

$$10 \text{ kg/hr} = 2.78 \text{ m/sec} (\approx 6 \text{ mph})$$

$$KE = \frac{1}{2} mV^2 = 15.4 \text{ KJ}$$

$$a = \frac{V^2}{2S} = 12.9 \text{ m/sec}^2$$

$$\text{Moon: } \frac{x}{h} = \frac{\frac{dV}{dt}}{g} = \frac{12.9}{1.6} = 8.1$$

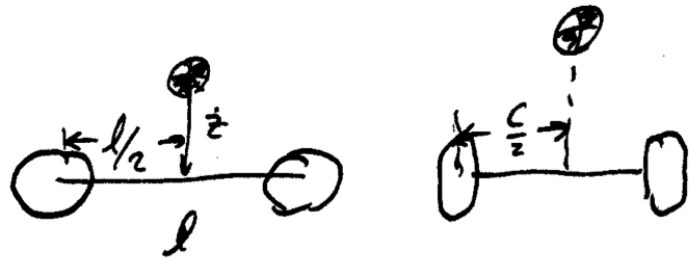
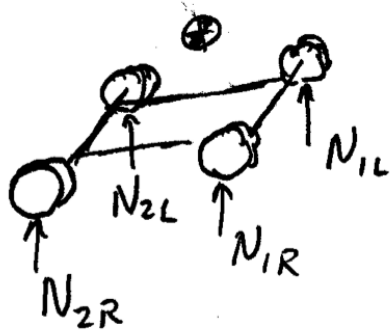
Assuming constant deceleration $F = ma =$

$$(4000 \text{ kg})(12.9 \text{ m/sec}^2) = 51.6 \text{ kN}$$

(11,600 lbs)

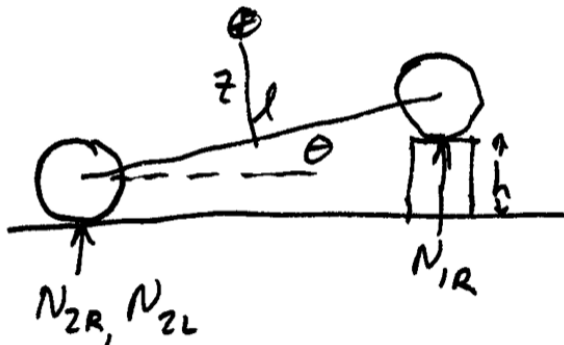
Static Forces on Rigid Suspension

4-wheeled cart



Level Ground: $N_{1R} = N_{2R} = N_{1L} = N_{2L} = \frac{W}{4}$

Obstacle under right front wheel



~~For~~ $N_{1L} = 0$
 (left front wheel
 dangling in air)

Force Equilibrium over an Obstacle

$$\sum M_{\text{back axle}} = N_{1R} l \cos \theta = W \left(\frac{l}{2} \cos \theta - z \sin \theta \right)$$

$$\sin \theta = \frac{h}{l} \quad \cos \theta = \sqrt{1 - \frac{h^2}{l^2}} \quad \text{Say, } h = \frac{3}{5}l \quad \uparrow \text{(arbitrary)}$$

$$\sin \theta = \frac{3}{5} \quad \cos \theta = \frac{4}{5} \quad z = \frac{l}{2} \quad \leftarrow$$

$$N_{1R} l \left(\frac{4}{5} \right) = W \left(\frac{l}{2} \frac{4}{5} - \frac{l}{2} \frac{3}{5} \right)$$

$$N_{1R} = \frac{5}{4} W \left(\frac{4}{10} - \frac{3}{10} \right) = \frac{W}{8} \quad \left(\text{was } \frac{W}{4} \right)$$

$$N_{2R} + N_{2L} = \frac{7}{8} W$$

Lateral Equilibrium

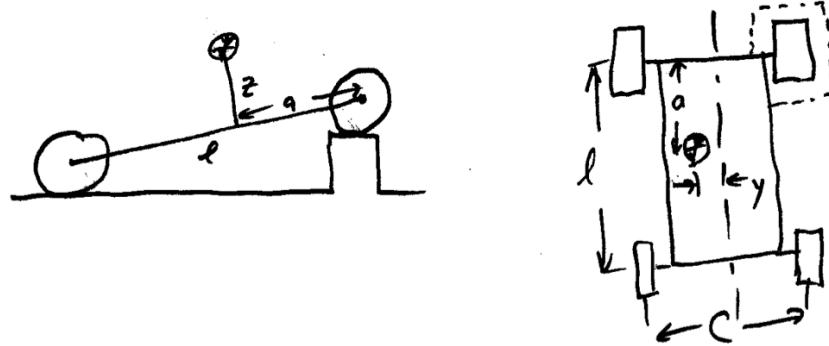
$$N_{2L} = N_{2R} + N_{1R} = \frac{1}{8} W + N_{2R} = \frac{W}{2}$$

$$\boxed{N_{1R} = \frac{W}{8}; \quad N_{2R} = \frac{3W}{8}; \quad N_{2L} = \frac{W}{2}}$$



Rigid Suspension - General Case

(Still has front right wheel on obstacle;
front left wheel off the ground)



Σ Moments about rear axle

$$N_{1R} l \cos \theta = W [(l-a) \cos \theta - z \sin \theta]$$

$$N_{1R} = W \left(\frac{l-a}{l} - \frac{z}{l} \tan \theta \right)$$

Σ Moments about centerline

$$N_{2L} \frac{c}{2} = (N_{1R} + N_{2R}) \frac{c}{2} + Wy$$

$$N_{2L} = N_{1R} + N_{2R} + \frac{2Wy}{c}$$

$$N_{2L} = W \left(\frac{l-g}{l} - \frac{z}{l} \tan \theta \right) + N_{2R} + \frac{2Wy}{c}$$

Σ Forces

$$N_{1R} + N_{2R} + N_{2L} = W$$

$$2W \left(\frac{l-g}{l} - \frac{z}{l} \tan \theta \right) + 2N_{2R} + \frac{2Wy}{c} = W$$

$$N_{2R} = \frac{W}{2} - W \left(\frac{l-g}{l} - \frac{z}{l} \tan \theta \right) - \frac{Wy}{c}$$

$$N_{2L} = \frac{W}{2} + \frac{Wy}{c}$$

$$N_{1R} = W \left(\frac{l-g}{l} - \frac{z}{l} \tan \theta \right)$$

$a = \frac{l}{2}$ $z = 0$ $y = 0$ (CG in plane of axes)

$$N_{2R} = \frac{W}{2} - \frac{W}{2} = 0 \quad N_{2L} = \frac{W}{2} \quad N_{1R} = \frac{W}{2} \quad N_{1L} = 0$$

$y \neq 0$

$$N_{2R} = -W \frac{y}{c} \quad N_{2L} = \frac{W}{2} + \frac{Wy}{c} \quad N_{1R} = \frac{W}{2}$$

if $y > 0$, $N_{2R} \rightarrow 0$

