

# Entry Aerodynamics

- Review of basic fluid parameters
- Heating rate parameters
- Stagnation point heating
- Heating on vehicle surfaces



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**Entry Heating**  
**ENAE 791 - Launch and Entry Vehicle Design**

# Basic Fluids Parameters

$$M \equiv \text{Mach Number} = \frac{v}{a}$$

$$a \equiv \text{speed of sound} = \sqrt{\gamma RT} \quad \left( R = \frac{\Re}{\bar{m}} \right)$$

$$\frac{\text{ordered energy}}{\text{random energy}} = \frac{\frac{1}{2}mv^2}{\frac{1}{2}m\bar{v}_g^2} = \frac{v^2}{3RT} = \frac{\gamma}{3} \frac{v^2}{a^2} = \frac{\gamma}{3} M^2$$

$$Re \equiv \text{Reynold's number} = \frac{\text{inertial force}}{\text{viscous force}}$$

$$Re = \frac{\dot{m}v}{\tau A} = \frac{\rho A v^2}{\mu \frac{v}{L} A} = \frac{\rho v L}{\mu}$$



# More Fluid Parameters

$K \equiv$  Knudsen number

$$K = \frac{\text{number of collisions with body}}{\text{number of collisions with other molecules}}$$

$$K = \frac{\lambda}{L}$$

$\lambda \equiv$  mean free path

$L \equiv$  vehicle characteristic length



# Prandtl Number

$$Pr = \mu \frac{C_p}{K}$$

where  $C_p \equiv$  specific heat at constant pressure

$K \equiv$  thermal conductivity

$\mu \equiv$  viscosity

$$Pr \propto \frac{\text{frictional dissipation}}{\text{thermal conduction}}$$

$Pr \approx 0.715$  for air at standard conditions





# Sutherland's Law (empirical)

- viscosity depends on temperature

$$\frac{\mu}{\mu_{ref}} = \left( \frac{T}{T_{ref}} \right)^{3/2} \frac{T_{ref} + S}{T + S}$$

$$\begin{aligned} \text{for air: } \mu_{ref} &= 1.789 \times 10^{-5} \frac{kg}{m \cdot sec} \\ T_{ref} &= 288 \text{ K} \\ S &= 110 \text{ K} \end{aligned}$$

- good to several thousand degrees



# Stanton Number

- applies to boundary layer problems

$$S_T = \frac{\dot{q}_w}{\rho_e v_e (H_{aw} - H_w)}$$

$H \equiv$  enthalpy

$= C_p T$  for perfect gas

$H_w =$  enthalpy at the wall

$H_{aw} =$  enthalpy at an adiabatic wall

$$\text{for } H_{aw}, \quad \left( \frac{\partial T}{\partial z} \right)_w = 0$$



# Approximating $H_{aw}$

$$H_o = H_e + \frac{u_e^2}{2} \quad \Leftarrow \text{total enthalpy at edge of boundary layer}$$

$$H_{aw} = H_e + r \frac{u_e^2}{2} \quad r \equiv \text{recovery factor}$$

$$H_{aw} = H_e + r(H_o - H_e)$$

for incompressible flow,  $r \approx \sqrt{Pr}$

$= 0.845$  for std. air

$r$  decreases only 2.4% from  $M=0$  to  $M=16$

$\implies$  fairly constant!



# Reynold's Analogy

$$\frac{S_T}{c_f} = \frac{1}{2} Pr^{-2/3}$$

$c_f \equiv$  skin friction coefficient

since  $Pr \approx 1$ ,  $S_T \approx \frac{c_f}{2} \quad \Leftarrow$  Reynold's Analogy



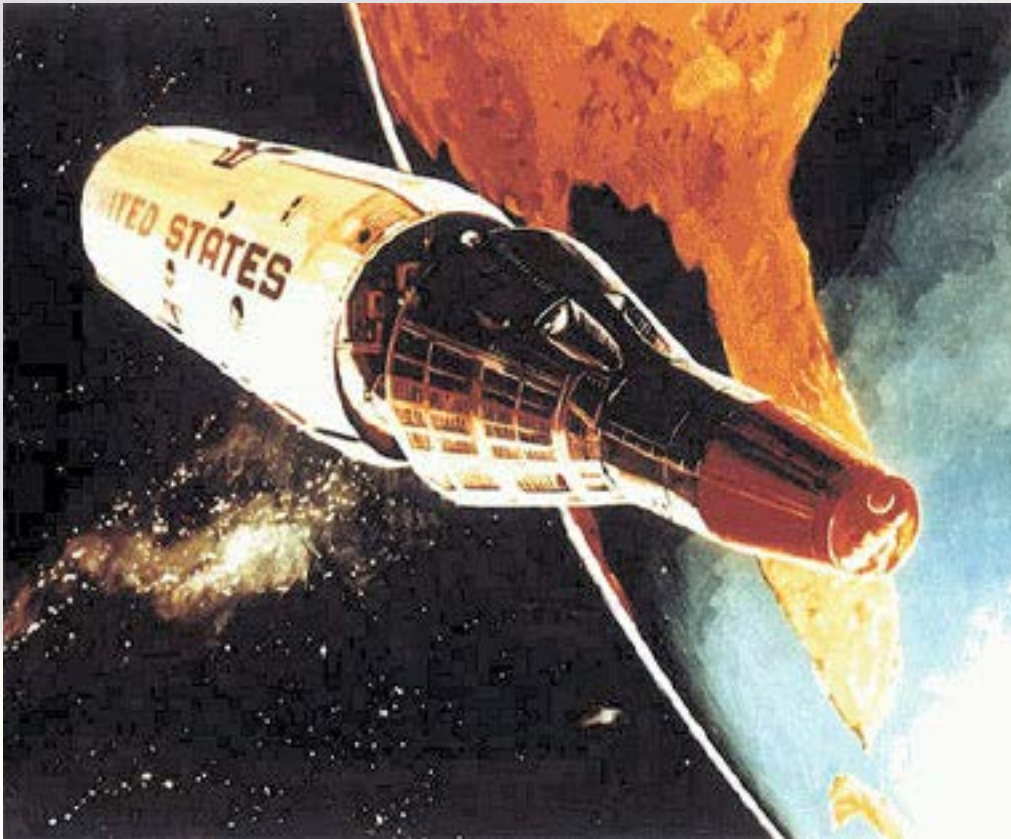


# Mercury Heat Shield Section



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# Gemini MOL Heat Shield





# Apollo 11 Heat Shield



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# Orion Heat Shield

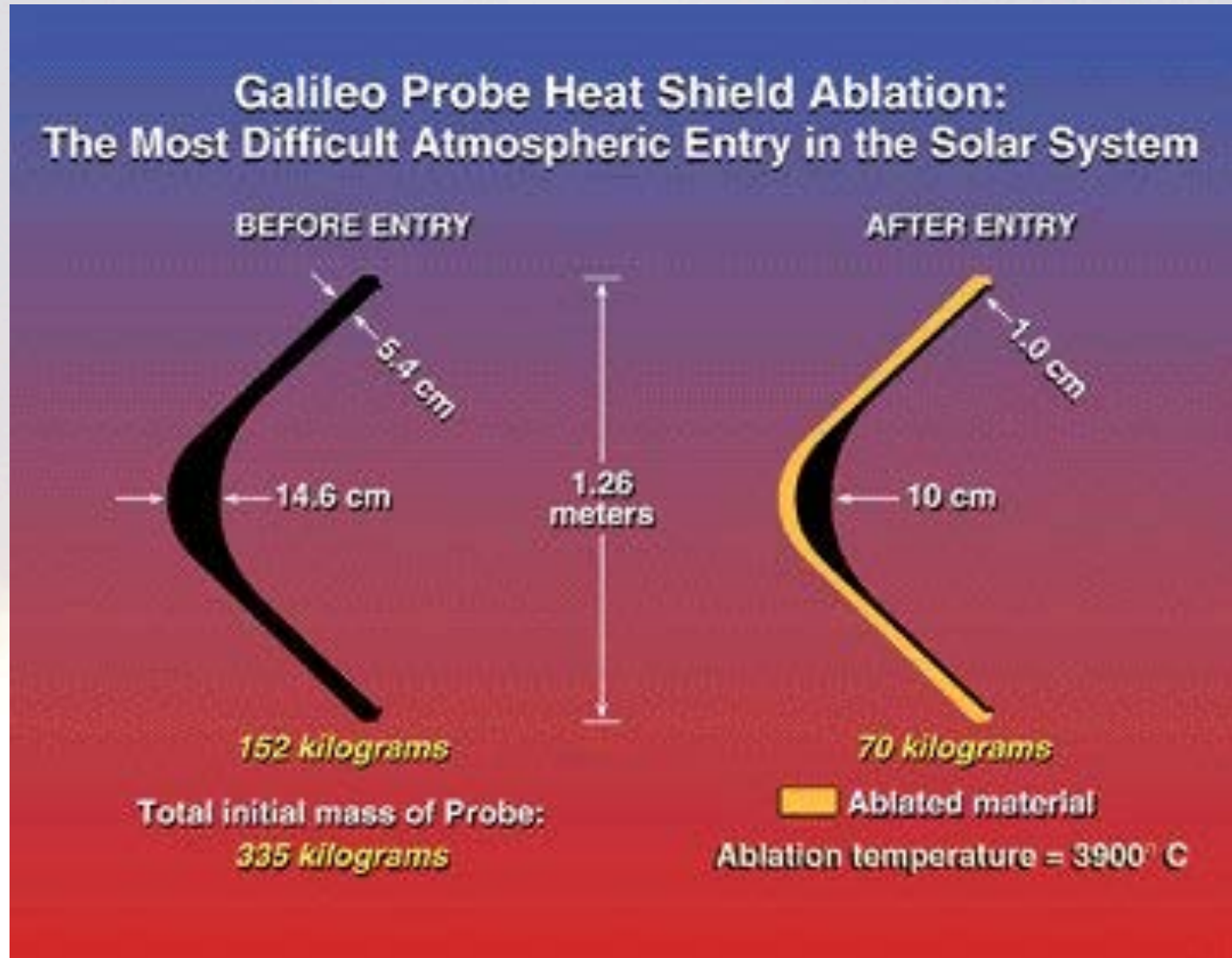


Phenolic Impregnated Carbon Ablator (PICA)

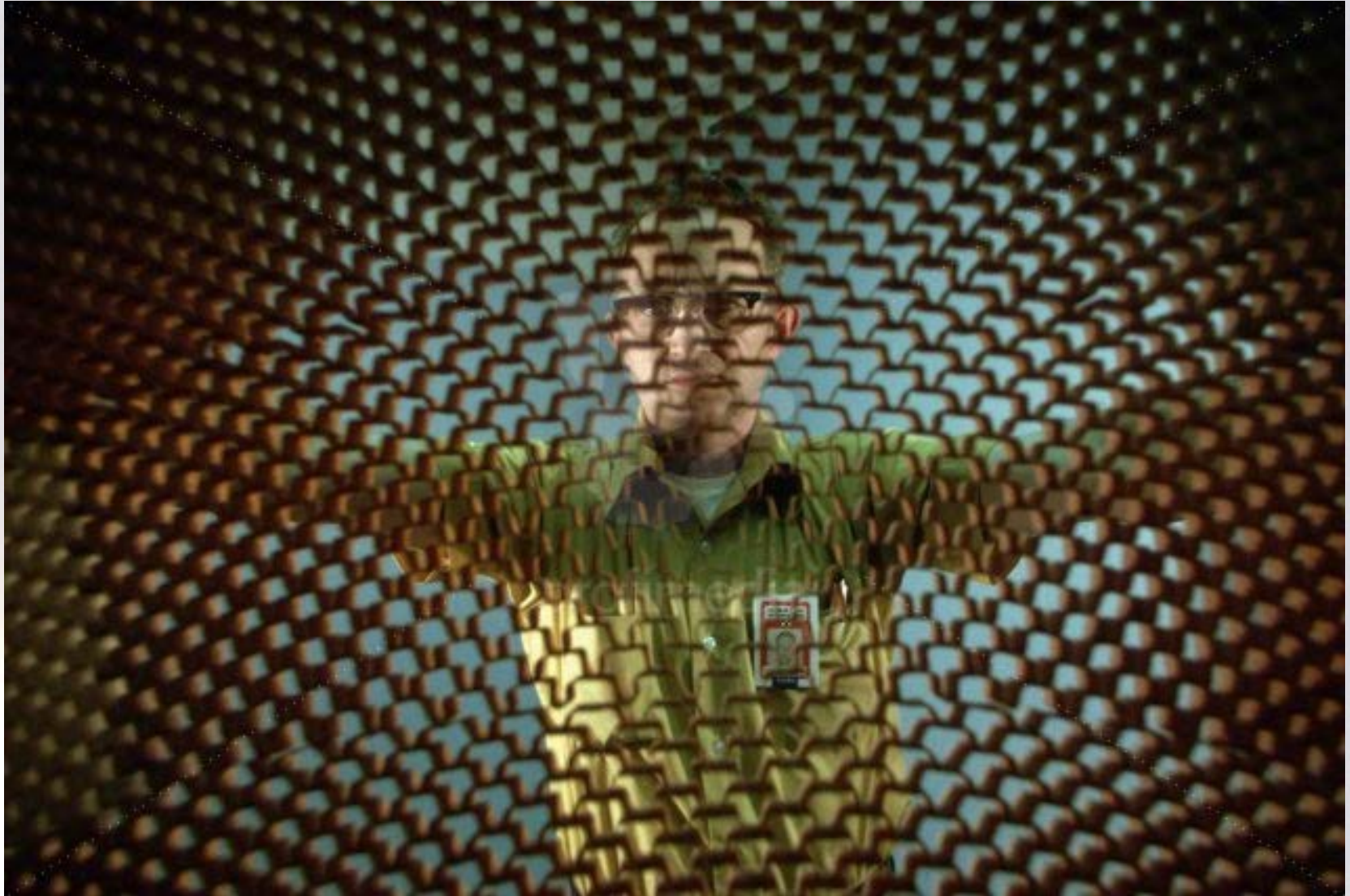




# Galileo Jupiter Probe Heat Shield



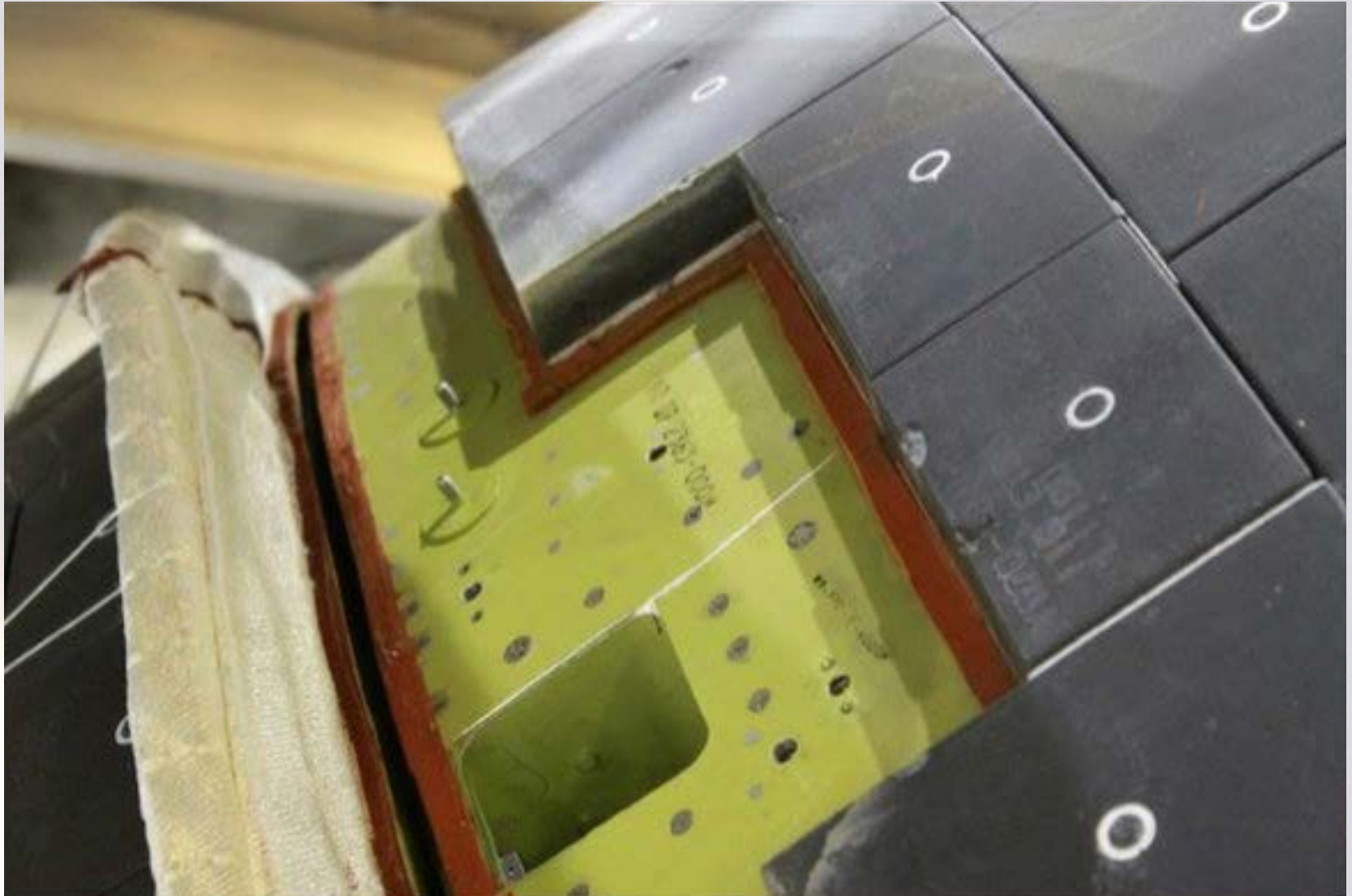
# Heat Shield Internal Structure



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# Shuttle Tile Installation



# Inflatable Heat Shield (Suborbital Test)

