# Terramechanics 1: Passive Rolling Resistance

- Origin and nature of lunar soil
- Soil mechanics
- Wheel-soil interactions
- Effects of tandem wheels

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# Lunar Regolith

- Broken down from larger pieces over time
- Major constituents
  - Rock fragments
  - Mineral fragments
  - Glassy particles
- Local environment
  - $10^{-12}$ torr (= $1.22 \times 10^{-10}$ Pa = $1.93 \times 10^{-14}$ psi)
  - Meteorites at velocities $>10^5$ m/sec
  - Galactic cosmic rays, solar particles
  - Temperature range +250°F – -250°F

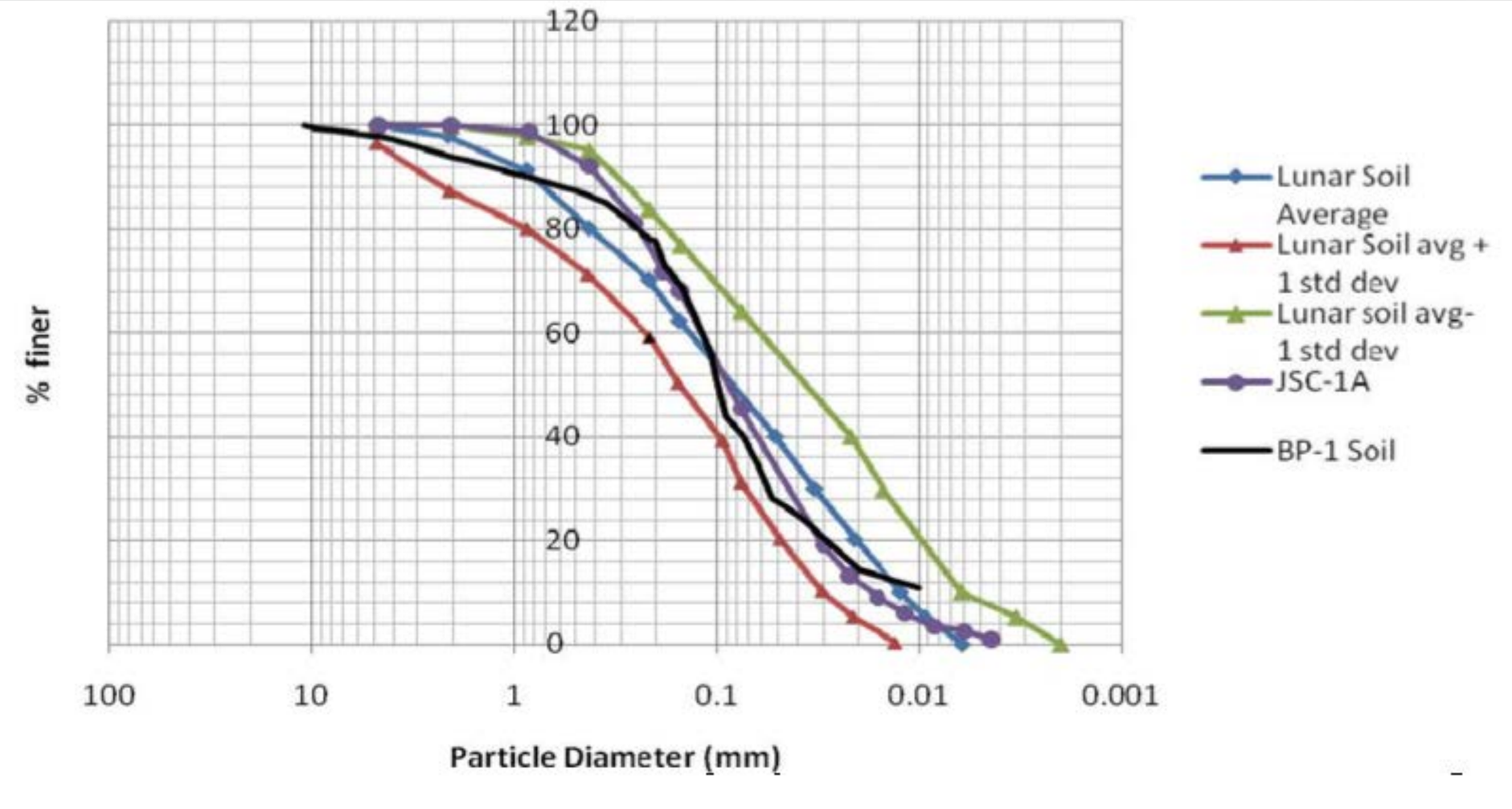
# Regolith Creation Process

- Only “weathering” phenomenon on the moon is meteoritic impact
- Weathering processes
  - Comminution: breaking rocks and minerals into smaller particles
  - Agglutination: welding fragments together with molten glass formed by impact energy
  - Solar wind spallation and implantation (minuscule)
  - Fire fountaining (dormant)

# JSC-1 Simulant

- Ash vented from Merriam Crater in San Francisco volcano field near Flagstaff, AZ
- K-Ar dated at 150,000 years old ± 30,000
- Major constituents $SiO_2$, $TiO_2$, $Al_2O_3$, $Fe_2O_3$, FeO, MgO, CaO, $Na_2O$, other <1%
- Represents low-Ti regolith from lunar mare
- MLS-1 simulant (U.Minn.) preferred for simulation of highland material
- BP-1 (Flagstaff, AZ) is ground basaltic lava - higher fidelity because of angular grain shapes

# Particle Size Distribution in Regolith




Rahmatian and Metzger, "Soil Test Apparatus for Lunar Surfaces" *Earth and Space 2010*, ASCE

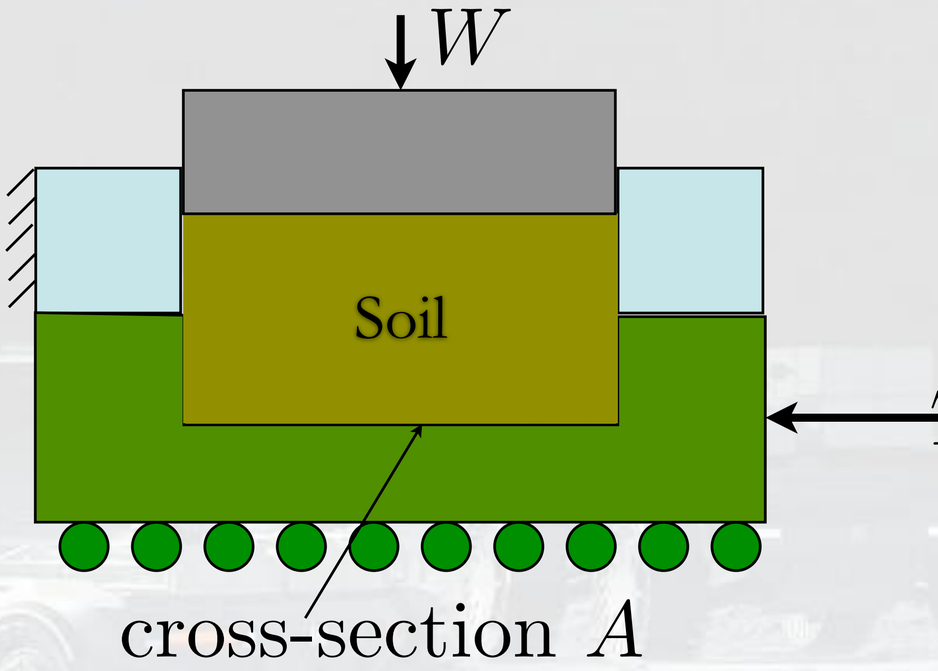
# Soil Testing Apparatus

Bevameter (force vs. displacement)

Internal friction angle φ

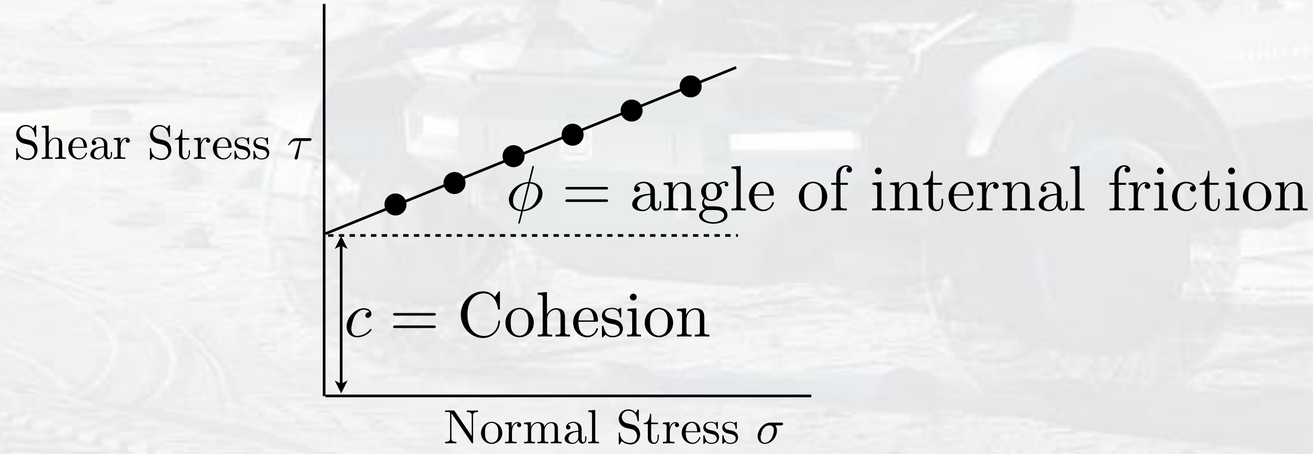
Shear deformation modulus K

# Soil Characterization – Direct Shear




$$\text{Shear Stress } \tau = \frac{T}{A}$$

$$\text{Normal Stress } \sigma = \frac{W}{A}$$



# Modeling Soil Reaction to a Wheel

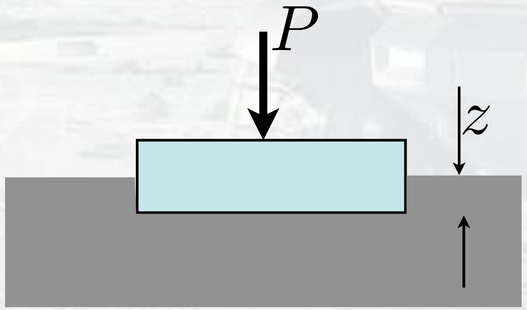
Assume soil reaction is like a (nonlinear) spring

$$P = kz^n$$

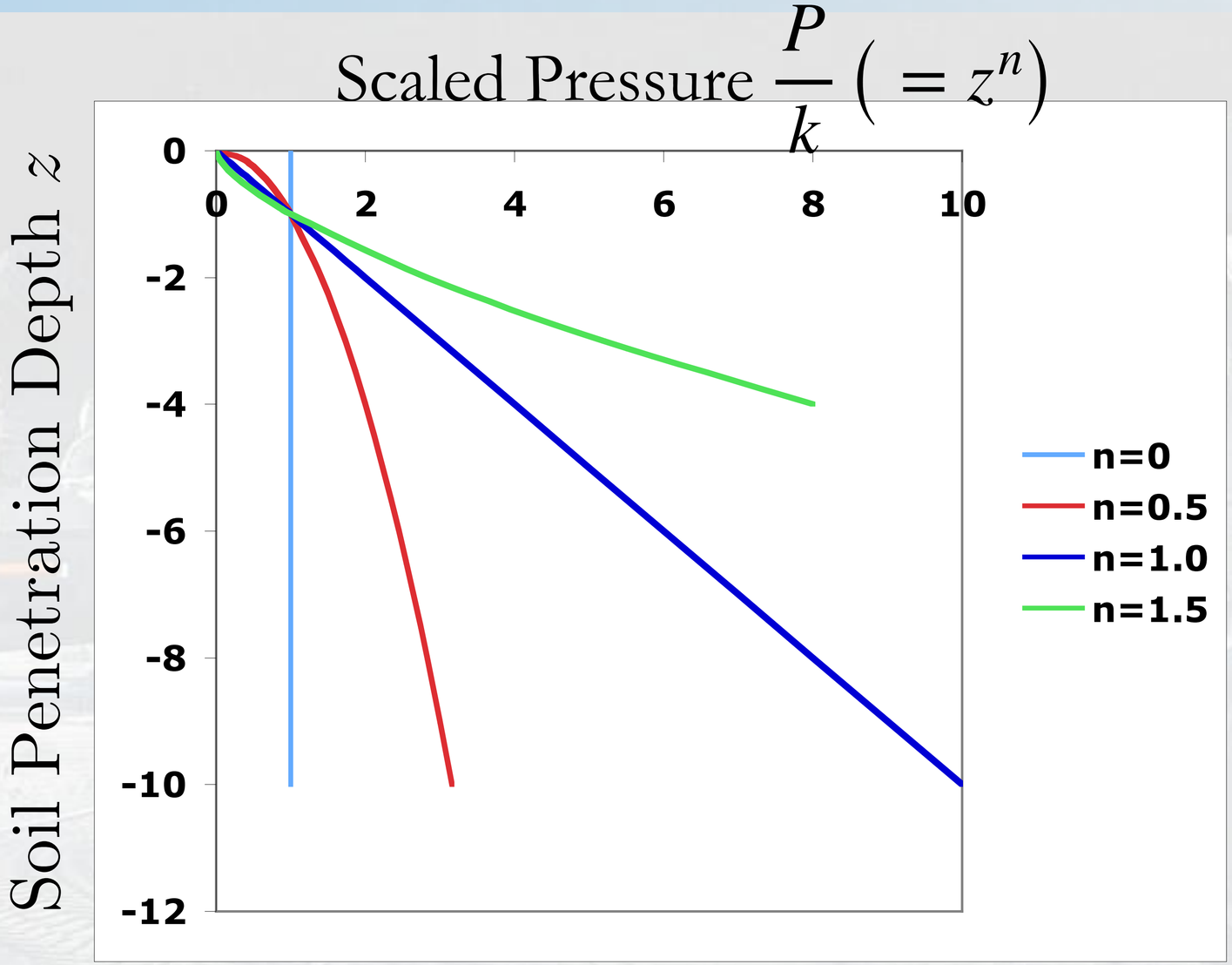
$P$ = applied pressure

$z$ = compression depth

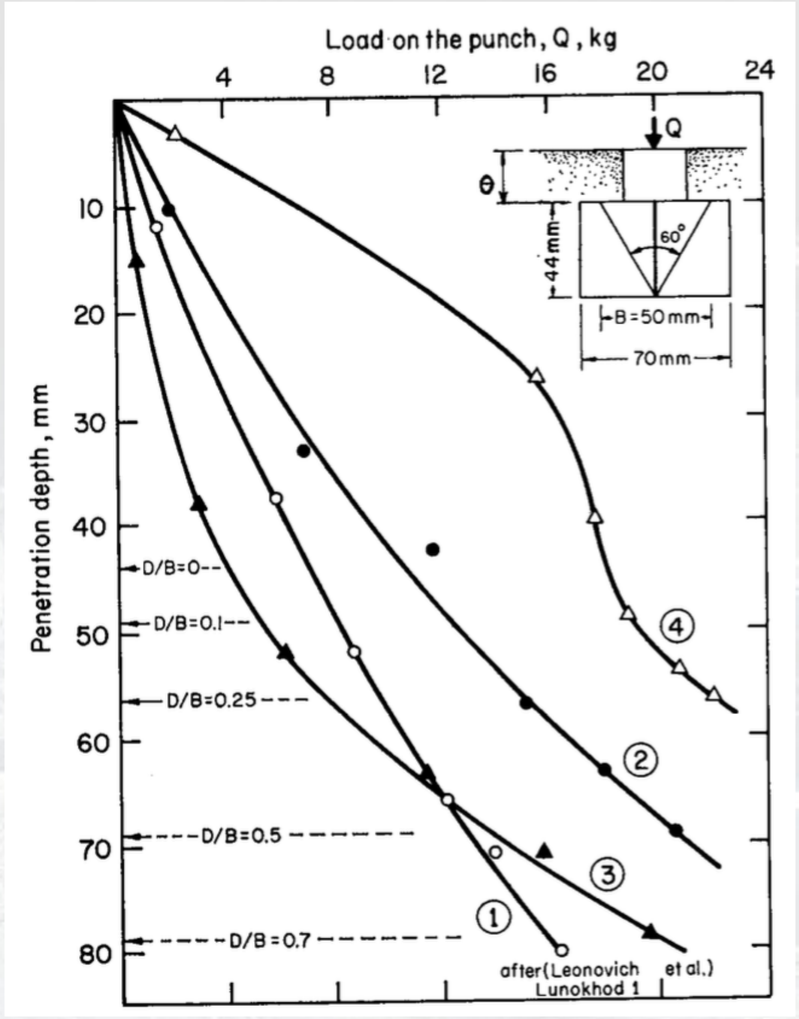
$k, n$ = heuristic parameters



# Effects of Soil Mechanics



# Lunokhod 1 Penetrometer Data



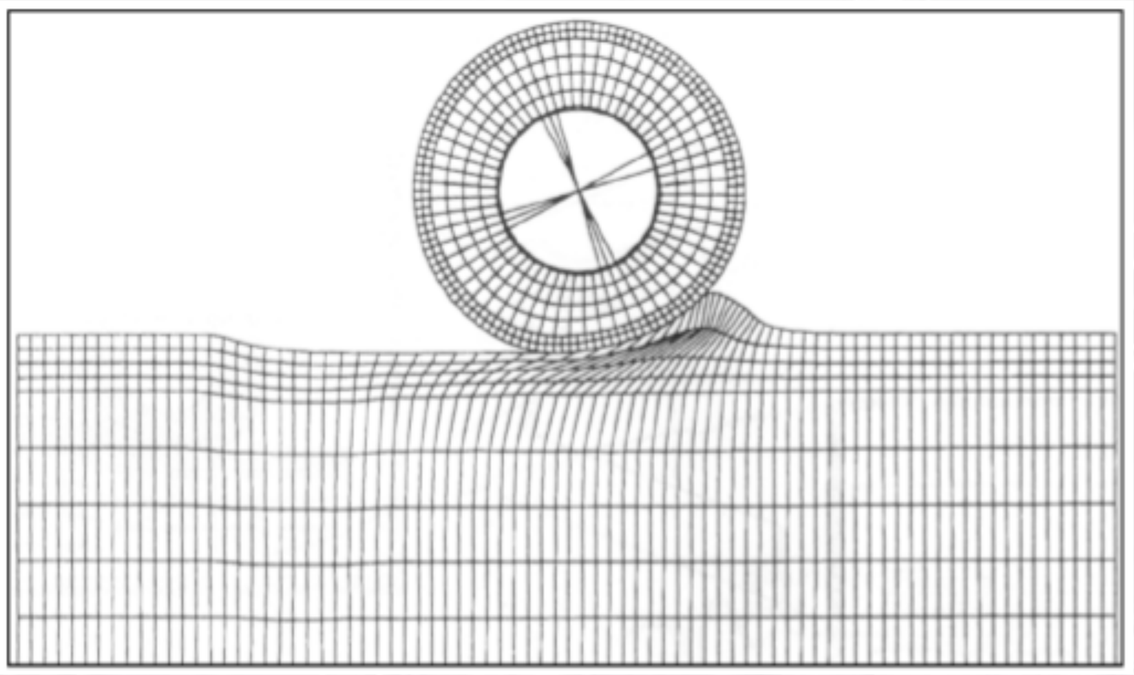

Mitchell et.al., Mechanical Properties of Lunar Soil: Density, Porosity, Cohesion, and Angle of Internal Friction"
Proceedings of the Third Lunar Science Conference, Vol. 3, MIT Press, 1972

# Wheel-Soil Interaction

Wheel rolling over soil does physical work

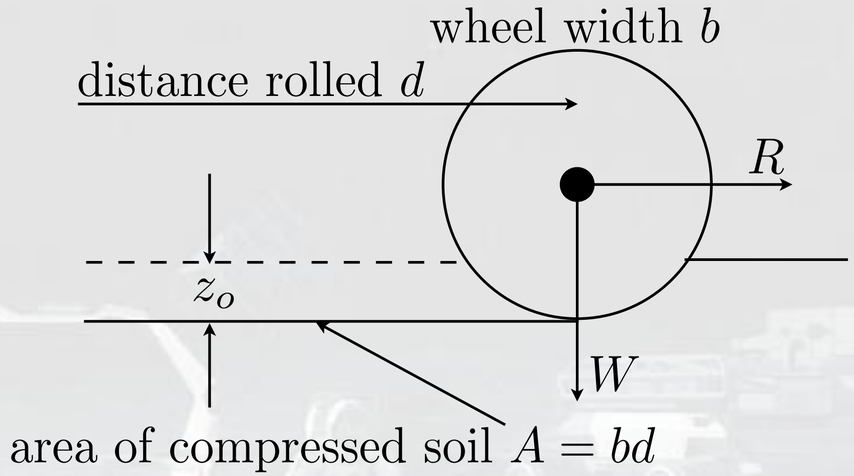
– Compression

– "Bulldozing"



from Gibbesch and Schafer, "Advanced and Simulation Methods of Planetary Rover Mobility on Soft Terrain" *8th ESA Workshop on Advanced Space Technologies for Robotics and Automation*, Noordwijk, The Netherlands, November, 2004

# Wheel-Soil Interactions




$$\text{Displacement Energy } \frac{E}{A} = \int \frac{F}{A} dz = \int P dz$$

$$\frac{E}{A} = \int_0^{z_o} P dz = \int_0^{z_o} k z^n dz = k \frac{z_o^{n+1}}{n+1}$$

# Rolling Resistance

$$\text{Total Energy } \frac{E}{A}A = \frac{E}{A}bd = k\frac{z_o^{n+1}}{n+1}bd$$

Given a force resisting rolling $\equiv R$,

the energy required to roll a distance d is

$$E_{roll} = Rd$$

$$E_{roll} = E_{displacement} \Rightarrow Rd = \frac{E}{A}bd$$

# Rolling Resistance

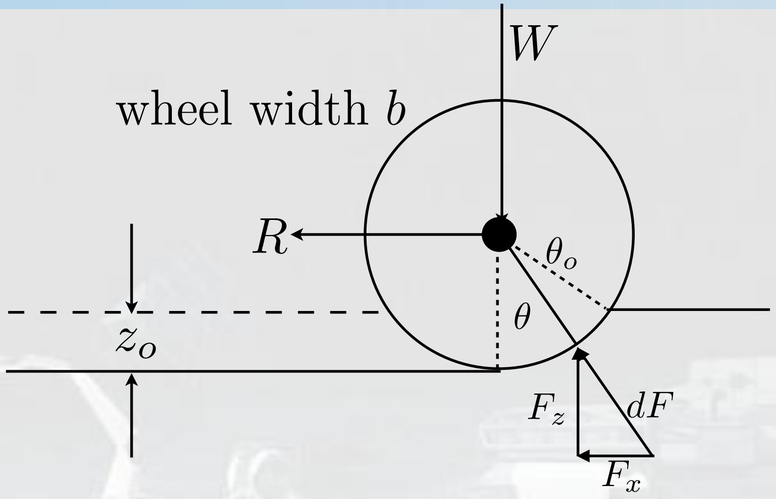
$$\text{For } n = 1 : P = kz; \frac{E}{A} = k\frac{z_o^2}{2}; R = \frac{1}{2}kbz_o^2$$

$$\text{For } n = \frac{1}{2} : P^2 = k^2 z; \frac{E}{A} = \frac{2}{3}kz_o^{\frac{3}{2}}; R = \frac{2}{3}kbz_o^{\frac{3}{2}}$$

$$\text{For } n = 0 : P = k; \frac{E}{A} = kz_o; R = kbz_o$$

$$\text{Generic case: } P = kz^n; \frac{E}{A} = k\frac{z_o^{n+1}}{n+1}; R = kb\frac{z_o^{n+1}}{n+1}$$

# Soil Displacement Calculations




$$R - \int_0^{\theta_o} dF \sin\theta = 0$$

$$-W + \int_0^{\theta_o} dF \cos\theta = 0$$

$$dF = Pbr\ d\theta$$

$$dF\cos\theta = -Pb\ dx$$

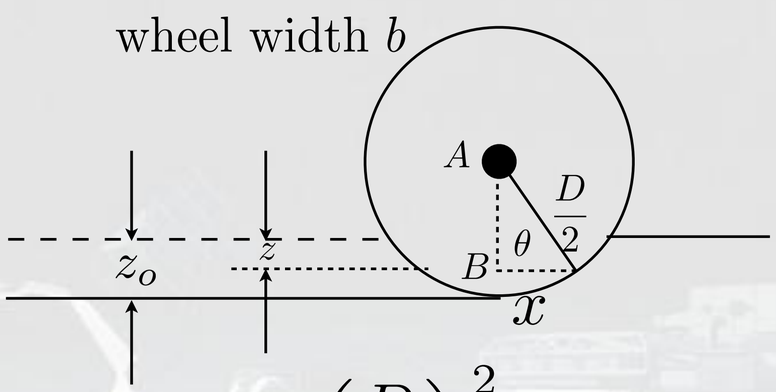
$$dF\sin\theta = Pb\ dz$$

$$R = \int_0^{\theta_o} Pb\ dz \qquad W = -\int_0^{\theta_o} Pb\ dx$$

In general, $P = kx^n$

$$W = -\int_0^{z_o} bkz^n dx$$

# Soil Displacement Calculations




$$\bar{AB} = \frac{D}{2} - (z_o - z)$$

$$x^2 = \left(\frac{D}{2}\right)^2 - \bar{AB}^2 = \left(\frac{D}{2}\right)^2 - \left[\frac{D}{2} - (z_o - z)\right]^2$$

$$= \left(\frac{D}{2}\right)^2 - \left(\frac{D}{2}\right)^2 + 2\frac{D}{2}(z_o - z) - (z_o - z)^2$$

$$x^2 = [D - (z_o - z)](z_o - z)$$

# Soil Compression Calculations

But $D \gg z_o - z$

$$x^2 \approx D(z_o - z) \Rightarrow 2x\ dx = -D\ dz$$

$$\text{so from } W = -\int_0^{z_o} bkz^n dx \text{ we get } W = -\int_0^{z_o} bkz^n \frac{-D}{2x} dz$$

$$W = -bk \int_0^{z_o} z^n \left( \frac{-D}{2\sqrt{D}\sqrt{z_o - z}} \right) dz$$

$$W = bk \int_0^{z_0} \left( \frac{\sqrt{D}}{2\sqrt{z_0 - z}} \right) z^n dz$$

# Soil Displacement Calculations

$$\text{Define } z_o - z \equiv t^2 \Rightarrow dz = -2tdt$$

$$W = bk\sqrt{D}\int_0^{\sqrt{z_o}} (z_o - t^2)^n dt$$

$$\text{Taylor Series expansion } (z_o - t^2)^n \cong z_o^n - nz_o^{n-1}t^2 + \cdots$$

$$W \approx \frac{bk\sqrt{Dz_o}}{3} z_o^n (3 - n)$$

$$\text{for } n = 1 \Rightarrow W = \frac{2}{3} bkz_o\sqrt{Dz_o}$$

$$\text{for } n = \frac{1}{2} \Rightarrow W = \frac{5}{6} bkz_o\sqrt{D}$$

$$\text{for } n = 0 \Rightarrow W = bk\sqrt{Dz_o}$$

# Rolling Resistance as f(W)

$$\text{for } n = 0 \Rightarrow W = bk\sqrt{Dz_o} \Rightarrow z_o = \left(\frac{W}{bk}\right)^2 \frac{1}{D}$$

$$R = kbz_o \Rightarrow R = \frac{kb}{(kb)^2}\frac{W^2}{D} \Rightarrow R = \frac{W^2}{kbD}$$

$$\text{for } n = \frac{1}{2} \Rightarrow W = \frac{5}{6}bkz_o\sqrt{D} \Rightarrow z_o = \frac{6}{5}\frac{W}{bk\sqrt{D}}$$

$$R = \frac{2}{3}kbz_o^{\frac{3}{2}} \Rightarrow R = \frac{2}{3}kb\left(\frac{6}{5}\frac{W}{kb\sqrt{D}}\right)^{\frac{3}{2}} = \frac{2}{3}\left(\frac{6}{5}\right)^{\frac{3}{2}}\frac{W^{\frac{3}{2}}}{\sqrt{kb}D^{\frac{3}{4}}}$$

$$R = 0.876\frac{W^{\frac{3}{2}}}{\sqrt{kb}D^{\frac{3}{4}}}$$

# Rolling Resistance as f(W)

$$\text{for } n = 1 \Rightarrow W = \frac{2}{3} b k z_o^{\frac{3}{2}} \sqrt{D} \Rightarrow z_o^2 = \left( \frac{3W}{2kb\sqrt{D}} \right)^{\frac{4}{3}}$$

$$R = \frac{1}{2} k b z_o^2 \Rightarrow R = \frac{1}{2} kb \left( \frac{3W}{2kb\sqrt{D}} \right)^{\frac{4}{3}} = \frac{1}{2} \left( \frac{3}{2} \right)^{\frac{4}{3}} \left( \frac{W^4}{kbD^2} \right)^{\frac{1}{3}}$$

$$R = 0.859 \left( \frac{W^4}{kbD^2} \right)^{\frac{1}{3}}$$

# Rolling Resistance as f(W) (Generic)

$$W = \frac{bk\sqrt{Dz_o}}{3} z_o^n (3-n) = \frac{bk\sqrt{D}}{3} z_o^{n+\frac{1}{2}} (3-n)$$

$$z_o^{n+\frac{1}{2}} = \frac{3}{(3-n)} \frac{W}{bk\sqrt{D}}$$

$$z_o^{n+1} = \left( \frac{3}{3-n} \frac{W}{bk\sqrt{D}} \right)^{\frac{n+1}{n+\frac{1}{2}}} = \left( \frac{3}{3-n} \frac{W}{bk\sqrt{D}} \right)^{\frac{2(n+1)}{2n+1}}$$

$$R = \frac{bk}{n+1} z_o^{n+1} = \frac{bk}{n+1} \left( \frac{3}{3-n} \frac{W}{bk\sqrt{D}} \right)^{\frac{2(n+1)}{2n+1}}$$

$$R = \frac{1}{n+1} \left( \frac{3}{3-n} \frac{W}{\sqrt{D}} \right)^{\frac{2(n+1)}{2n+1}} \left( \frac{1}{bk} \right)^{\frac{1}{2n+1}}$$

# Soil Characteristics

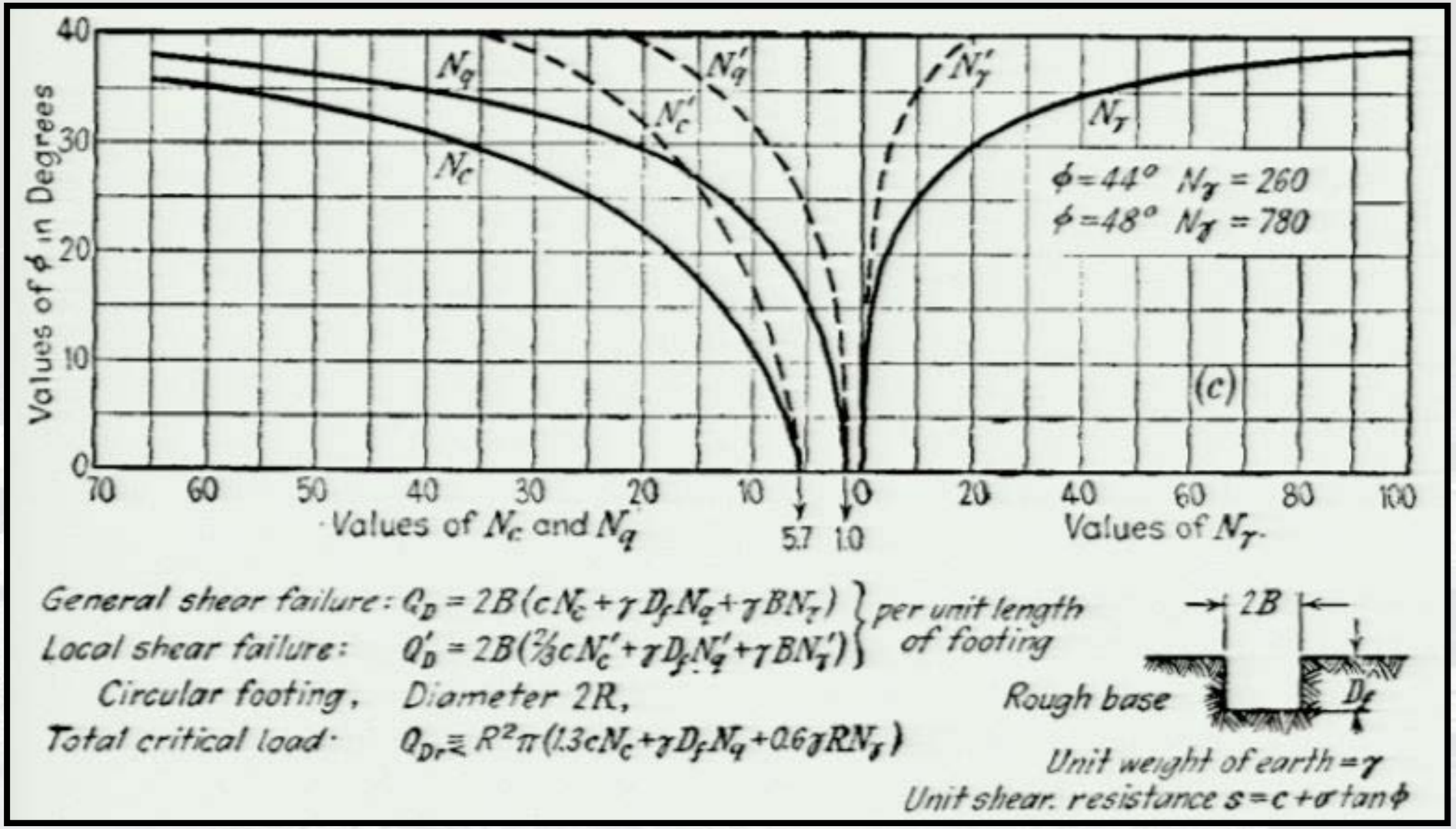
| soil type | n | $k_c \left\langle \frac{N}{m^{n+1}} \right\rangle$ | $k_\phi \left\langle \frac{N}{m^{n+2}} \right\rangle$ |
|---|---|---|---|
| Dry Sand | 1.1 | 990 | 1,528,000 |
| Lunar Regolith | 1 | 1400 | 820,000 |
| Sandy Loam | 0.7 | 5270 | 1,515,000 |
| Sandy Loam (MER-B) | 1 | 28,000 | 7,600,000 |
| Slope Soil (MER-B) | 0.8 | 6800 | 210,000 |
| Clay (Earth) | 0.5 | 13,190 | 692,200 |

# More Earth Soil Characteristics

| Terrain | n | $k_c$ ($kN/m^{n+1}$) | $k_\varphi$ ($kN/m^{n+2}$) | c (kPa) | φ (deg) |
|---|---|---|---|---|---|
| Dry Sand | 1.1 | 0.99 | 1528.43 | 1.04 | 28 |
| Sandy Loam | 0.7 | 5.27 | 1515.04 | 1.72 | 29 |
| Sandy Loam | 0.2 | 2.56 | 43.12 | 1.38 | 38 |
| Sandy Loam | 0.9 | 52.53 | 1127.97 | 4.83 | 20 |
| Sandy Loam | 0.4 | 11.42 | 808.96 | 9.65 | 35 |
| Sandy Loam | 0.3 | 2.79 | 141.11 | 13.79 | 22 |
| Sandy Loam | 0.5 | 0.77 | 51.91 | 5.17 | 11 |
| Clayey Soil | 0.5 | 13.19 | 692.15 | 4.14 | 13 |
| Clayey Soil | 0.7 | 16.03 | 1262.53 | 2.07 | 10 |
| Heavy Clay | 0.13 | 12.7 | 1555.95 | 68.95 | 34 |
| Heavy Clay | 0.11 | 1.84 | 103.27 | 20.69 | 6 |
| Lean Clay | 0.2 | 16.43 | 1724.69 | 68.95 | 20 |
| Lean Clay | 0.15 | 1.52 | 119.61 | 13.79 | 11 |
| LETE Sand | 0.79 | 102 | 5301 | 1.3 | 31.1 |
| Upland Sandy Loam | 1.1 | 74.6 | 2080 | 3.3 | 33.7 |
| Rubicon Sandy Loam | 0.66 | 6.9 | 752 | 3.7 | 29.8 |
| North Gower Clayey Loam | 0.73 | 41.6 | 2471 | 6.1 | 26.6 |
| Grenville Loam | 1.01 | 0.06 | 5880 | 3.1 | 29.8 |
| Snow (USA) | 1.6 | 4.37 | 196.72 | 1.03 | 19.7 |
| Snow (USA) | 1.6 | 2.49 | 245.9 | 0.62 | 23.2 |
| Snow (Sweden) | 1.44 | 10.55 | 66.08 | 6 | 20.7 |

D. Michel and K. McIsaac, "New Rocker-Bogie and Terramechanics-Based Wheel/Soil Interaction Models for Planetary Rovers" 2012 International Conference On Mechatronics and Automation

# Terzaghi Analysis of Soil Deformation



# Terzaghi Soil Bearing Capacity Factors

$$N_q = \frac{\exp\left[\left(\frac{3\pi}{2} - \phi\right)\tan\phi\right]}{2\cos^2\left(\frac{\pi}{4} + \frac{\phi}{2}\right)}$$

$$N_c = \cot\phi\left\{\frac{\exp\left[\left(\frac{3\pi}{2} - \phi\right)\tan\phi\right]}{2\cos^2\left(\frac{\pi}{4} + \frac{\phi}{2}\right)} - 1\right\} = \frac{N_q - 1}{\tan\phi}$$

$$N_\gamma = \frac{2(N_q + 1)\tan(\phi)}{1 + 0.4\sin(4\phi)}$$

$\phi$ = Angle of internal resistance of soil

# Parameter Definition

$K_c \equiv$ Cohesive modulus of soil deformation

$$K_c = (N_c - \tan\phi)\cos^2\phi$$

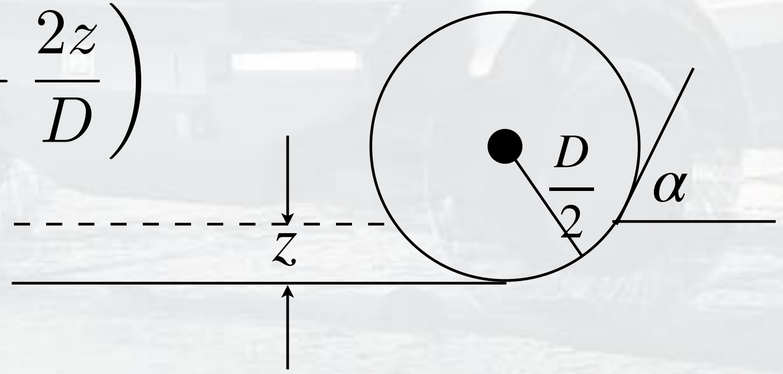
$K_\phi \equiv$ Frictional modulus of soil deformation

$$K_\gamma = \left[\frac{2N_\gamma}{\tan\phi} + 1\right]\cos^2\phi$$

$\alpha \equiv$ Angle of approach of wheel to soil

$$\alpha = \cos^{-1}\left(1 - \frac{2z}{D}\right)$$

$\gamma \equiv$ Weight density of soil $\left(\frac{N}{m^3}\right)$



# Lunar Soil Canonical Values

$$\text{Soil density: } \rho = 1600 \ \frac{kg}{m^3} \Longrightarrow \gamma = 2470 \ \frac{N}{m^3}$$

$$n = 1$$

$$k_c = 1400 \ N/m^2$$

$$k_\phi = 830{,}000 \ N/m^3$$

$$\phi = 33^{\circ} = 0.576 \ rad$$

$$\text{Cohesion } c = 170 \ N/m^2$$

$$N_q = 32.23$$

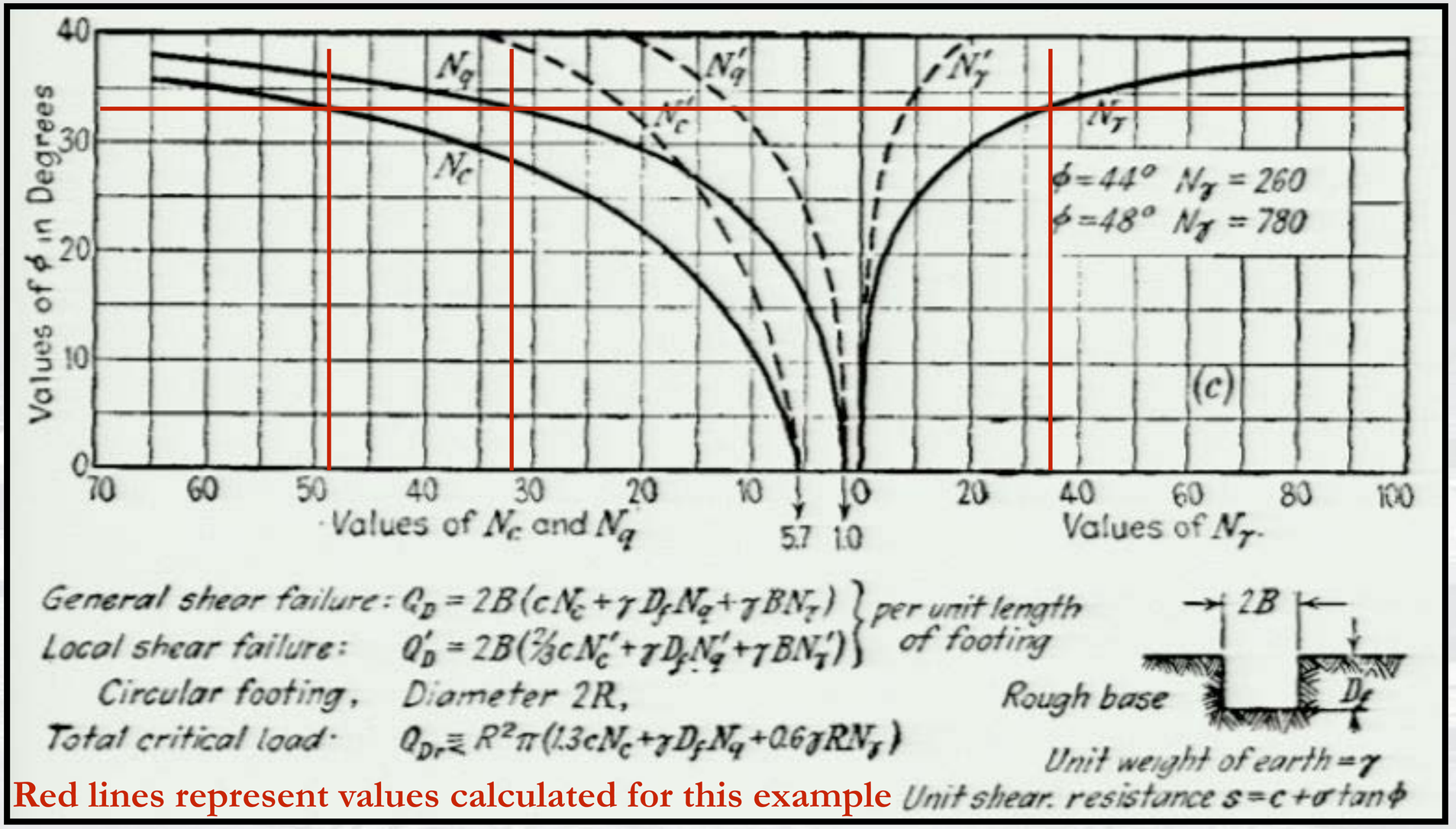
$$N_c = 48.09$$

$$N_\gamma = 33.27$$

$$K_c = 33.37$$

$$K_\phi = 72.77$$

# LRV Terzhagi Parameters




Red lines represent values calculated for this example

# More Detailed Soil Compression Equation

$$k = \frac{k_c}{b} + k_\phi$$

$k_c$ = modulus of cohesion of soil deformation

$k_c$ units $\Rightarrow < N/m^{(n+1)} >$

$k_\phi$ = modulus of friction of soil deformation

$k_\phi$ units $\Rightarrow < N/m^{(n+2)} >$

$b$ = wheel width

$$\boxed{P = \left(\frac{k_c}{b} + k_\phi\right) z^n}$$

# Equations for Compression Resistance

From page 21,

$$z = \left( \frac{3}{3-n} \frac{W_w}{bk\sqrt{D}} \right)^{\frac{2}{2n+1}}$$

$$W_w = \text{weight on wheel}$$

$$D = \text{wheel diameter}$$

$$R_c = \left( \frac{bk}{n+1} \right) z^{n+1}$$

$$R_c = \text{compression resistance (per wheel)}$$

$$k = \frac{k_c}{b} + k_\phi \Longrightarrow bk = k_c + bk_\phi$$

# Equations for Compression Resistance

$$z = \left( \frac{3}{3-n} \frac{W_w}{(k_c + bk_\phi)\sqrt{D}} \right)^{\frac{2}{2n+1}}$$

$$R_c = \left( \frac{k_c + bk_\phi}{n+1} \right) z^{n+1}$$

$$R_c = \left( \frac{k_c + bk_\phi}{n+1} \right) \left( \frac{3}{3-n} \frac{W_w}{(k_c + bk_\phi)\sqrt{D}} \right)^{\frac{2(n+1)}{2n+1}}$$

# Compression Resistance (Lunar Soil)

$$R_c = \frac{1}{n+1}(k_c + bk_\phi)^{\frac{-1}{2n+1}}\left(\frac{3W_w}{(3-n)\sqrt{D}}\right)^{\frac{2(n+1)}{2n+1}}$$

$$n = 1$$

$$z = \left(\frac{3}{2}\frac{W_w}{(k_c + bk_\phi)\sqrt{D}}\right)^{\frac{2}{3}}$$

$$R_c = \frac{1}{2}(k_c + bk_\phi)^{\frac{-1}{3}}\left(\frac{3W_w}{2\sqrt{D}}\right)^{\frac{4}{3}}$$

# Relevant LRV Parameters

$$W_w = 370\ lbs = 168\ kg = 259\ N \text{ (on Moon)}$$

$$D = 32\ in = 0.813\ m$$

$$b = 9\ in = 0.229\ m$$

$$z = \left( \frac{3}{2} \frac{259\ N}{\left(1400\ \frac{N}{m^2} + (0.229\ m) 830000\ \frac{N}{m^3}\right)\sqrt{0.813\ m}} \right)^{\frac{2}{3}} = 0.0151\ m$$

Units check: $\left( \frac{N}{(\frac{N}{m^2} + \frac{Nm}{m^3})\sqrt{m}} \right)^{\frac{2}{3}} = \left( m^{\frac{3}{2}} \right)^{\frac{2}{3}} = m$

# Soil Bearing Limit

Safe weight on the soil

$$W_s = A\left(cN_c + \gamma z N_q + \frac{1}{2}\gamma b N_\gamma\right)$$

Safe soil pressure $P_s = \dfrac{W_s}{A}$

$c \equiv$ Soil cohesion $(Pa)$

$b \equiv$ Wheel width $(m)$

For our LRV example case, $P_s = 18{,}790\ Pa$

For $W_v = 1004\ N$, the minimum contact area is $534\ cm^2$ or $\ell > 5.8\ cm$

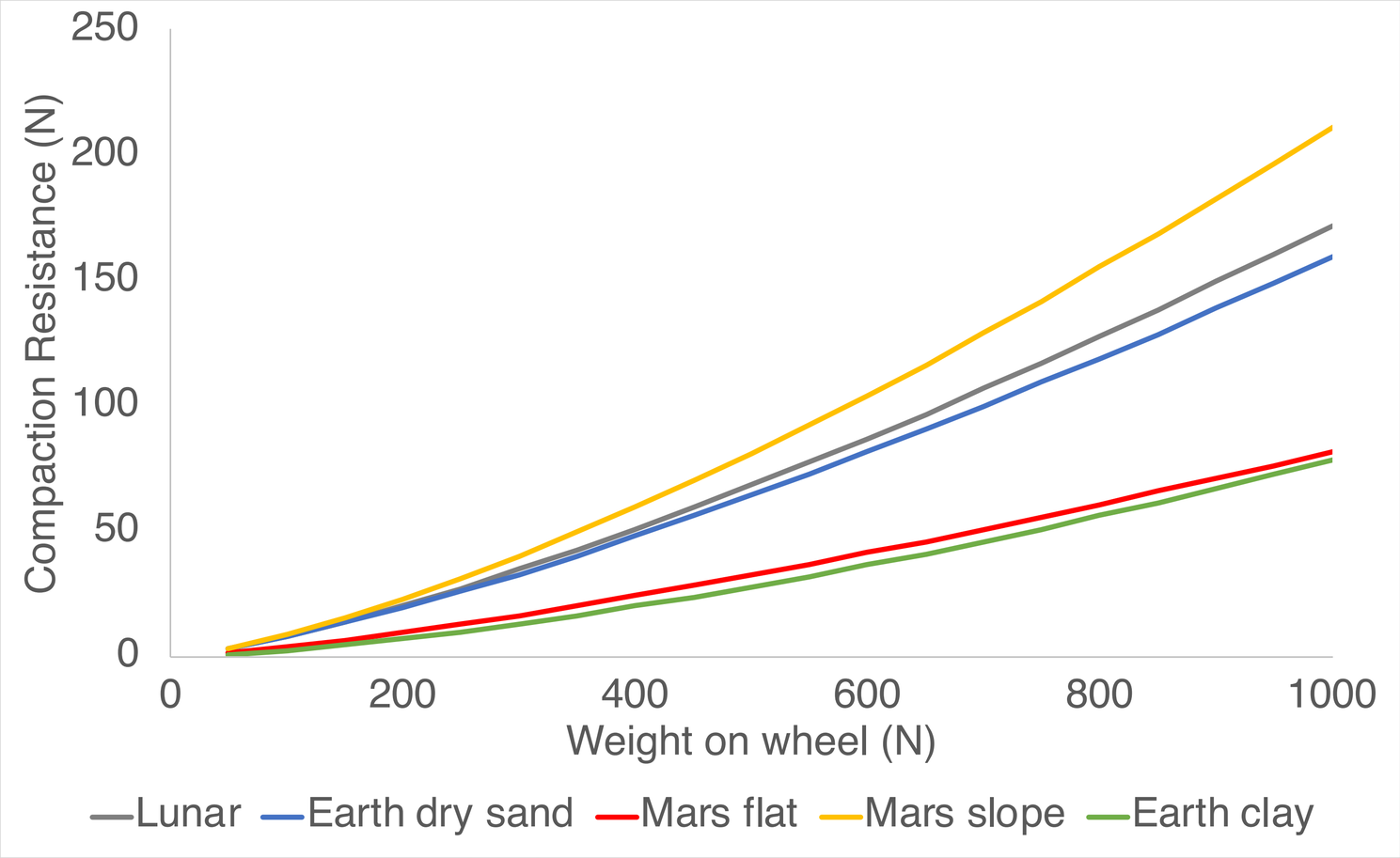
# LRV Compression Resistance

$$R_c = \frac{1}{2}\left(1400\ \frac{N}{m^2} + (0.229\ m)820000\ \frac{N}{m^3}\right)^{\frac{-1}{3}}\left(\frac{3(259\ N)}{2\sqrt{0.813\ m}}\right)^{\frac{4}{3}} = 28.3\ N$$

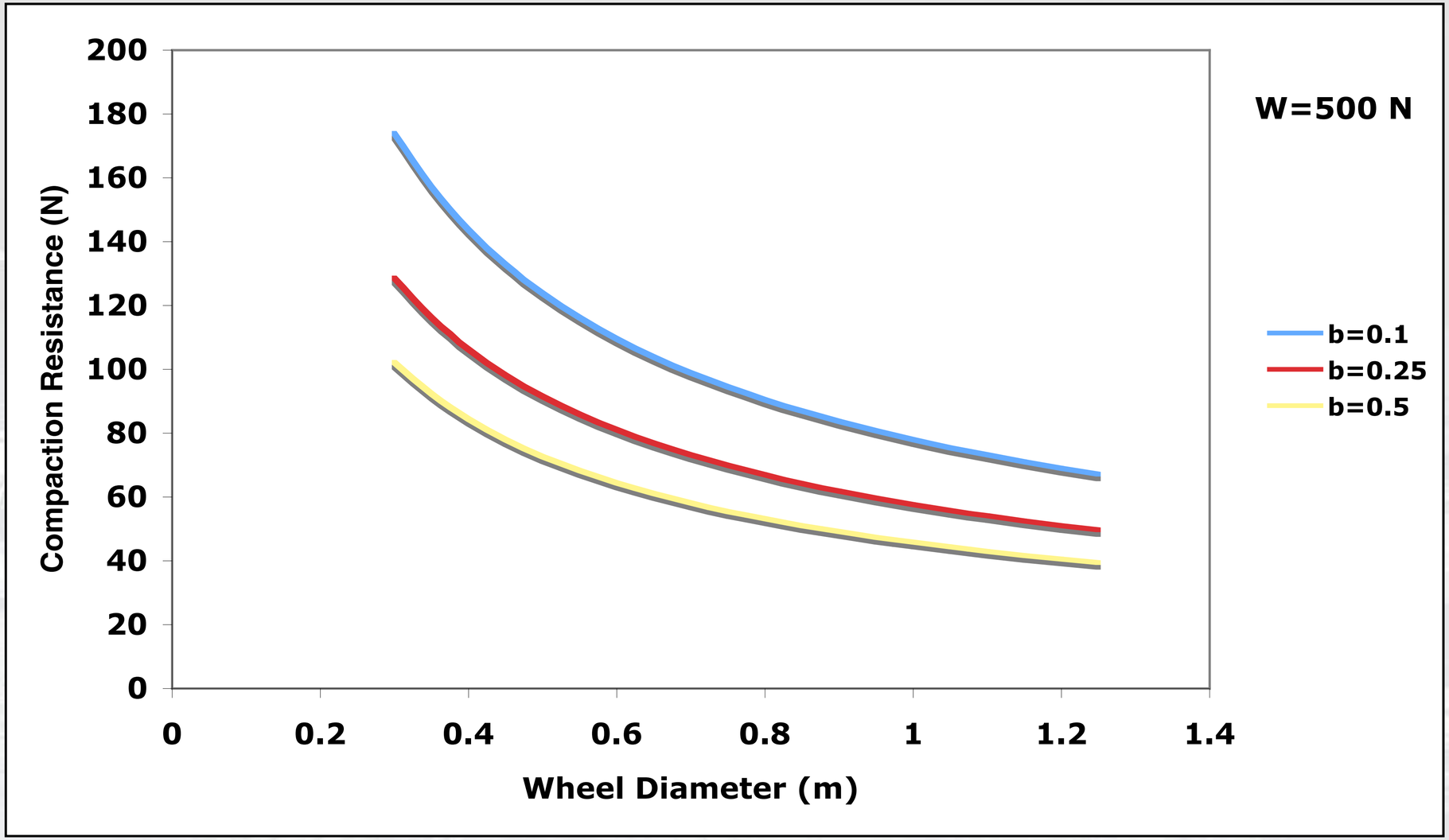
Check units: $$\left(\frac{N}{m^2} + \frac{Nm}{m^3}\right)^{\frac{-1}{3}}\left(\frac{N}{\sqrt{m}}\right)^{\frac{4}{3}} = \left(\frac{m^{2/3}}{N^{1/3}}\right)\left(\frac{N^{4/3}}{m^{2/3}}\right) = N$$

# LRV Wheel - Different Weights and Soils

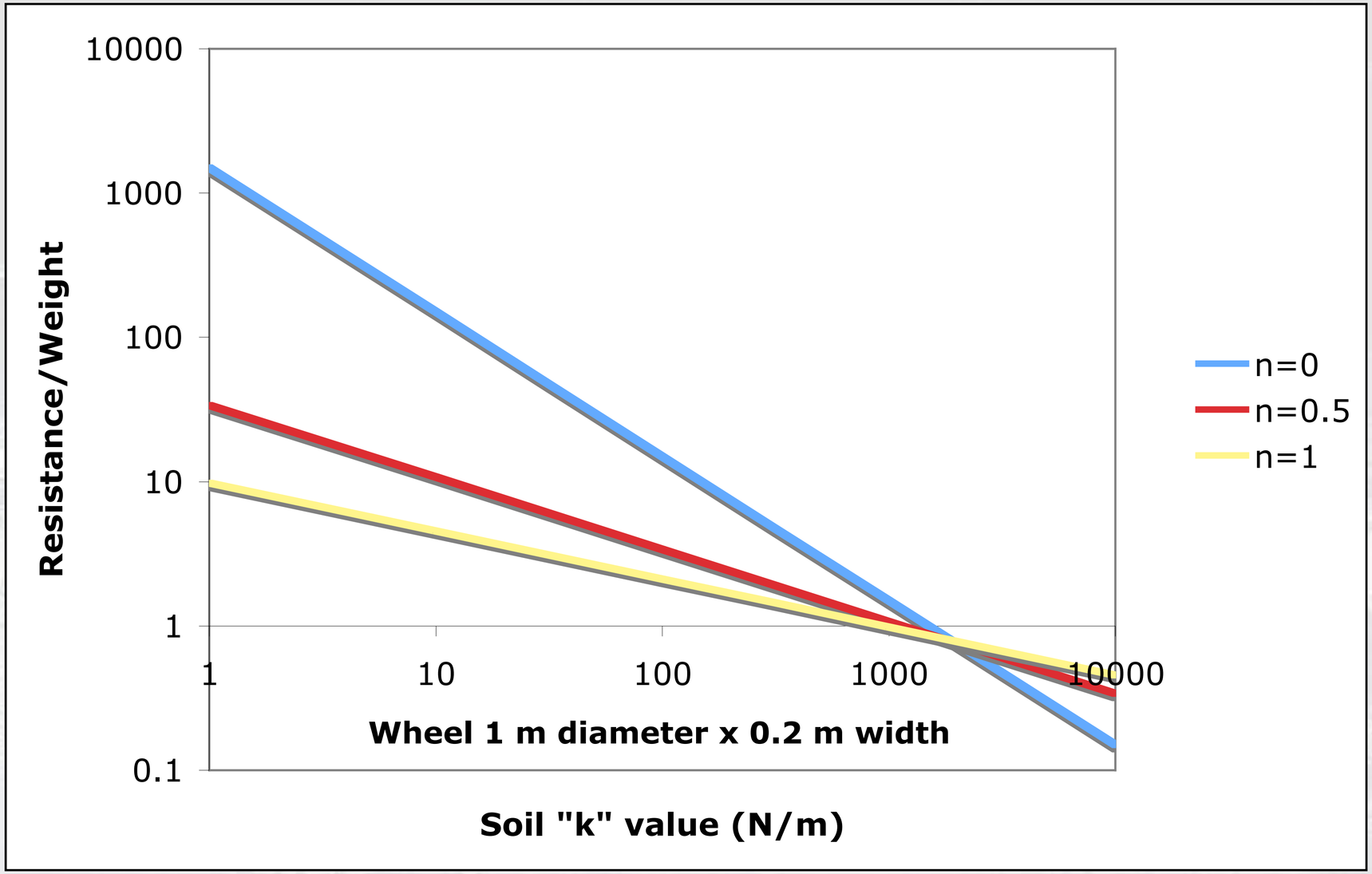
$$R = (k_c + k_\phi b)^{\frac{-1}{2n+1}} W^{\frac{2(n+1)}{2n+1}} \frac{1}{n+1} \left( \frac{3}{3-n} \right)^{\frac{2(n+1)}{2n+1}} D^{\frac{-(n+1)}{2n+1}}$$



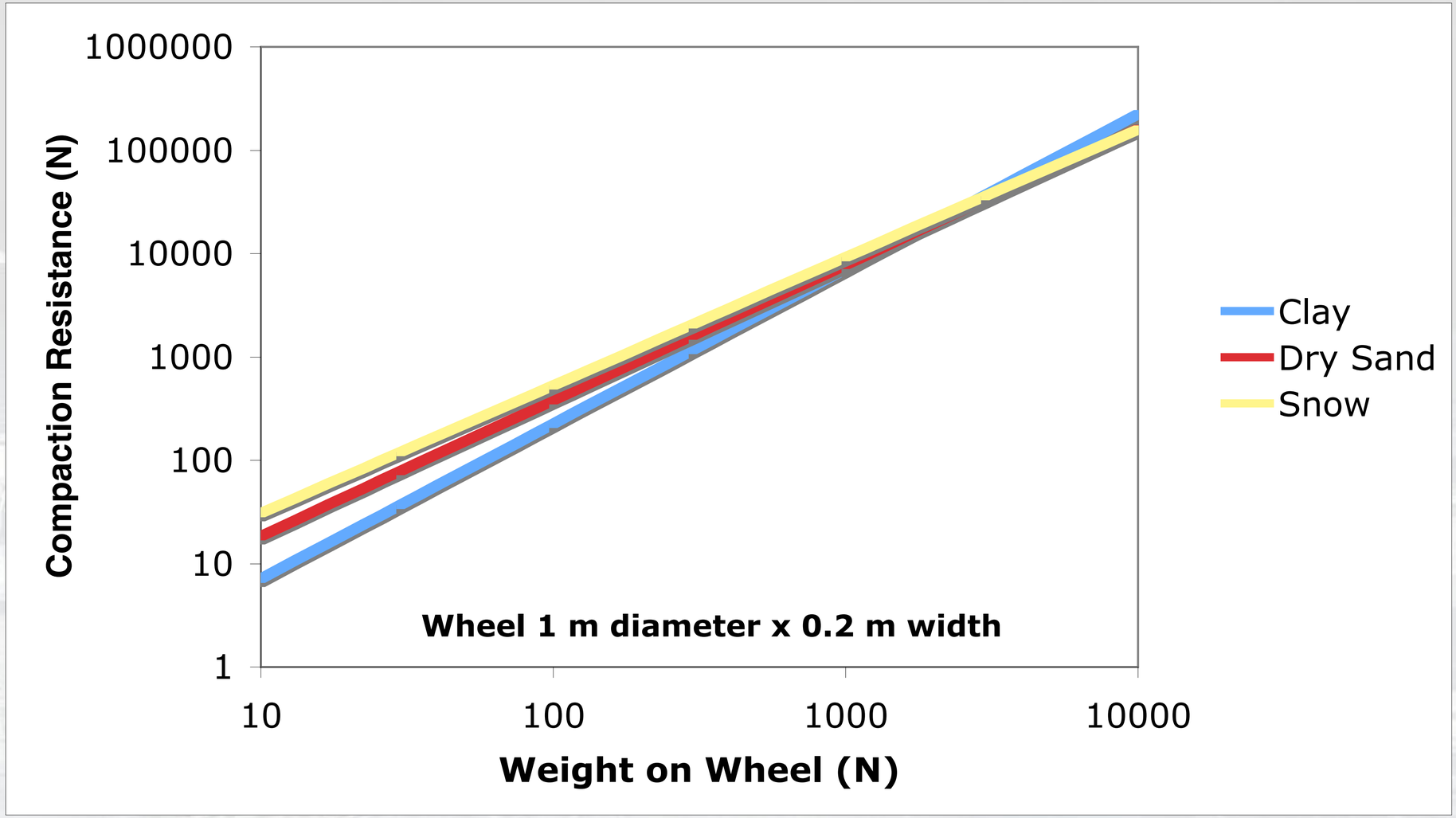
# Effects of Wheel Parameters



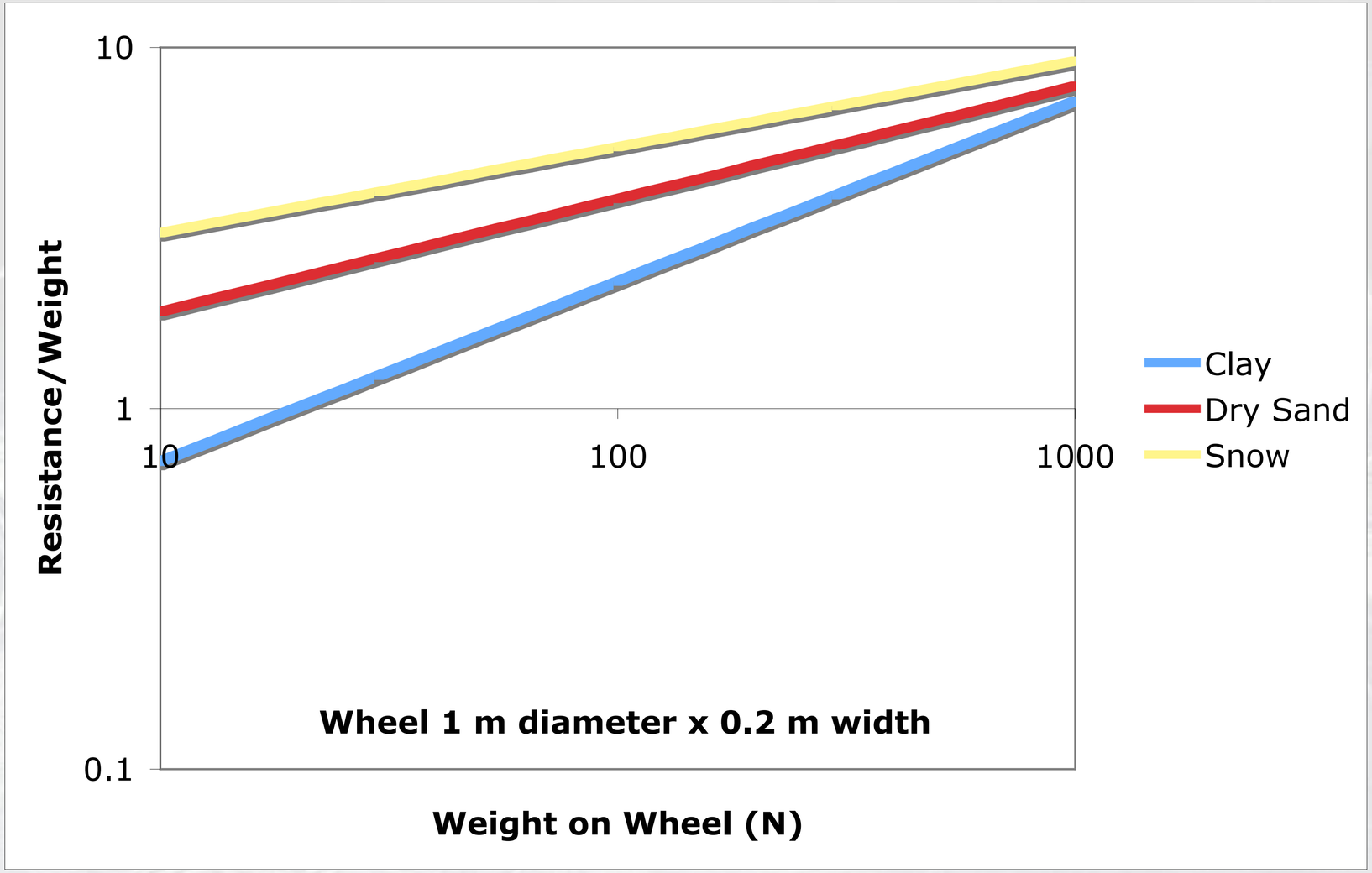
# Effect of Soil "Spring Constant" on R/W



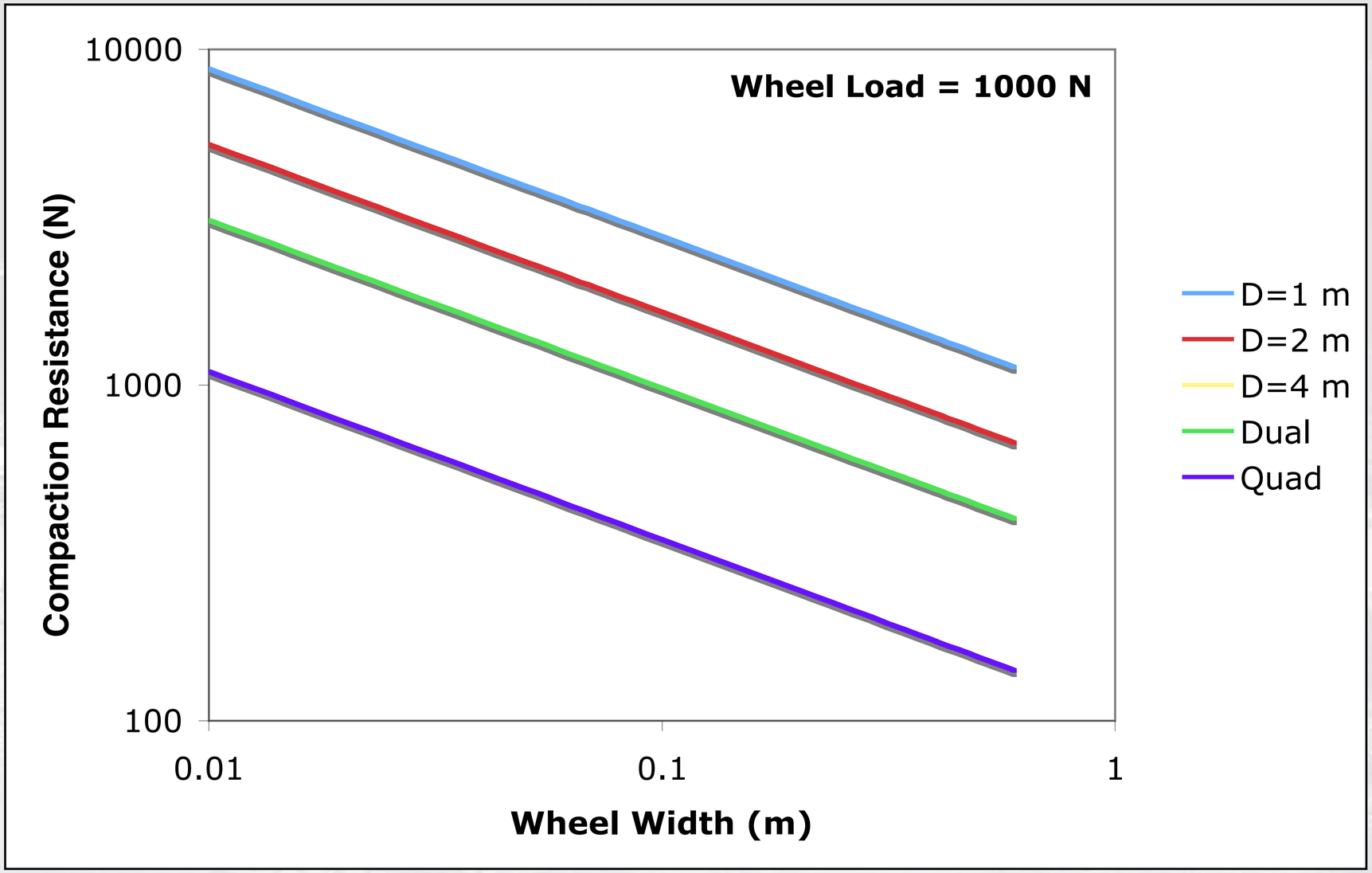
# Soil Type and Wheel Load



# Soil Type and Specific Resistance



# Effect of Wheel Diameter and Width



# Rolling and Gravitation Resistance

- Rolling resistance (tires, bearings, etc.)

$$R_r = W_v c_f$$

$$W_v = \text{weight of vehicle}$$

$$c_f = \text{coefficient of friction (typ. } 0.05)$$

- Gravitational resistance

$$R_g = W_v \sin\theta_{slope}$$

- LRV examples (15° slope, $W_v$=1004 N)

$$R_r = 50\ N \qquad R_g = 260\ N$$

# Bulldozing Resistance

General case:

$$R_b = \frac{b \sin(\alpha + \phi)}{2 \sin\alpha \cos\phi} \left(2zcK_c + \gamma z^2 K_\gamma\right) + \frac{\ell_o^3 \gamma}{3}\left(\frac{\pi}{2} - \phi\right) + c\ell_o^2\left[1 + \tan\left(\frac{\pi}{4} + \frac{\phi}{2}\right)\right]$$

*All angles in radians!*

$$\alpha = \text{angle of attack of wheel in soil} \equiv \cos^{-1}\left(1 - \frac{2z}{D}\right)$$

$$\gamma = \text{density of soil} \left\langle \frac{N}{m^3} \right\rangle \qquad \ell_o = z\tan^2\left(\frac{\pi}{4} - \frac{\phi}{2}\right)$$

For tracked vehicles, only the first term applies:

$$R_b = \frac{b \sin(\alpha + \phi)}{2 \sin\alpha \cos\phi} \left(2zcK_c + \gamma z^2 K_\gamma\right)$$

# LRV Bulldozing Example (1)

$$\phi = 33^o = 0.576\ rad$$

$$\alpha = \cos^{-1}\left(1 - \frac{2z}{D}\right) = \cos^{-1}\left(1 - \frac{2(1.812)}{81.2}\right) = 17.18^\circ = 0.2999 \text{ rad}$$

$$\ell_o = z\tan^2\left(\frac{\pi}{4} - \frac{\phi}{2}\right) = 0.0051\ m$$

$\ell_o$ is length of soil ruptured by compression

Soil parameter values calculated on page 26

$$\ell = \frac{D}{2}\cos^{-1}\left(1 - \frac{2z}{D}\right) = 12.18 \text{ cm}$$

$\ell$ is the length of the wheel's circumference in contact with the soil

# LRV Bulldozing Example (2)

$$R_b = \frac{b \sin(\alpha + \phi)}{2 \sin\alpha \cos\phi} \left(2zcK_c + \gamma z^2 K_\gamma\right) + \frac{\ell_o^3 \gamma}{3}\left(\frac{\pi}{2} - \phi\right) + c\ell_o^2 \left[1 + \tan\left(\frac{\pi}{4} + \frac{\phi}{2}\right)\right]$$

$$\langle R_b \rangle = cm\left(cm\ \frac{N}{cm^2} + \frac{N}{cm^3} cm^2\right) + cm^3 \frac{N}{cm^3} + \frac{N}{cm^2} cm^2$$

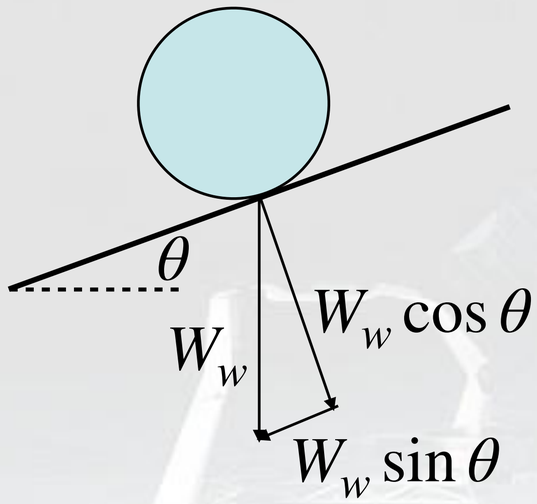
$$R_b = 94.98 + 0.000131 + 0.014 = 95.00\ N \text{ per leading wheel}$$

$$R_{b,total} = 190.0\ N$$

# Total LRV Rolling Resistance Estimate

- Compression resistance $R_c$ (4 wheels) 113 N
- Rolling resistance $R_r$ 50 N
- Bulldozing resistance $R_b$ (2 front wheels) 190 N
- *Total resistance, flat ground* *352 N*
- Gravitational resistance, 15° slope 260 N
- *Total resistance, 15° slope* *613 N*

# Revisiting Rolling Resistance and Slopes




LRV example - $n = 1$

$$R_c = \frac{1}{2}(k_c + bk_\phi)^{\frac{-1}{3}}\left(\frac{3W_w \cos\theta}{2\sqrt{D}}\right)^{\frac{4}{3}}$$

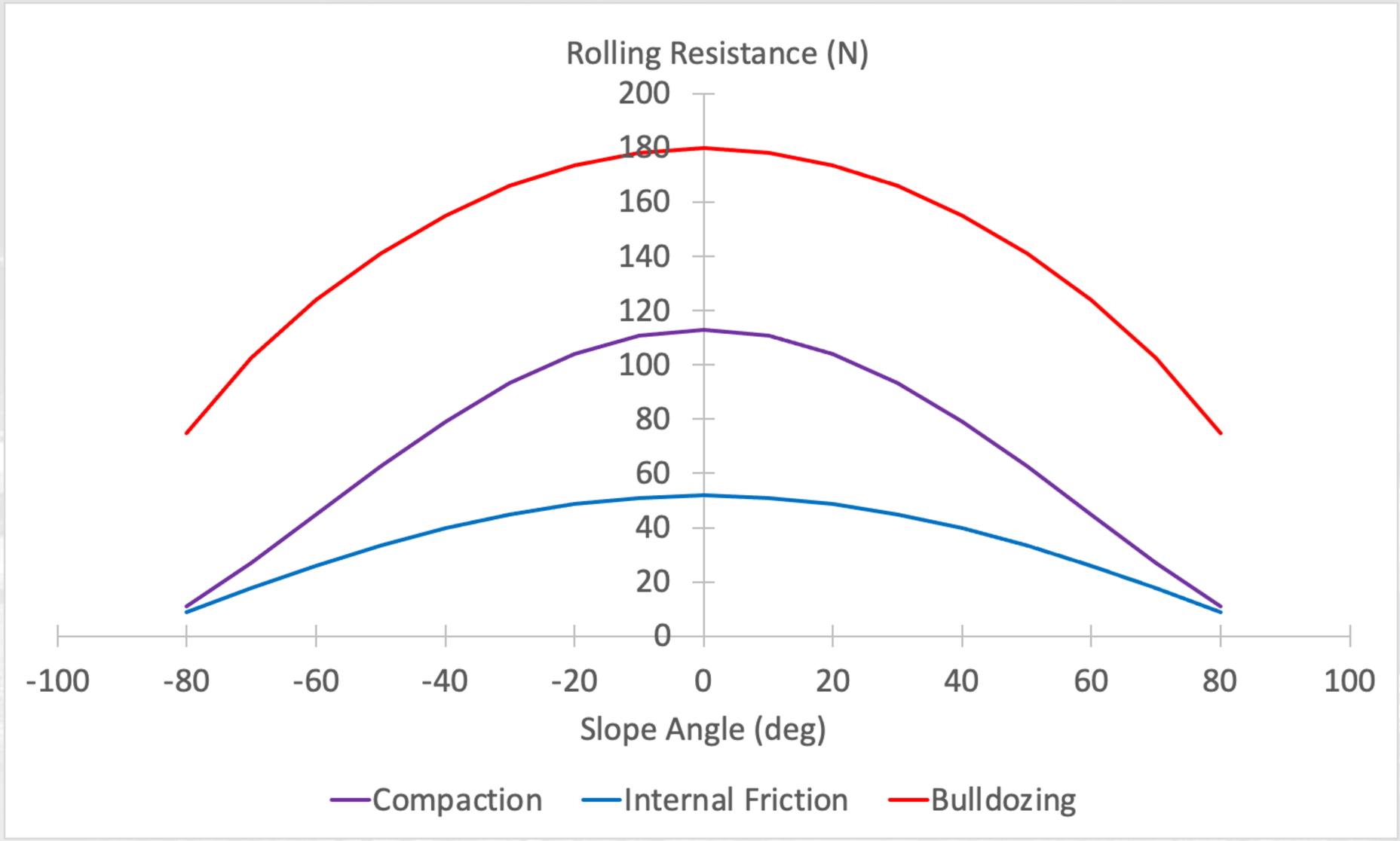
$$R_g = W_v \sin\theta$$

$$R_r = W_v \cos\theta \; c_f$$

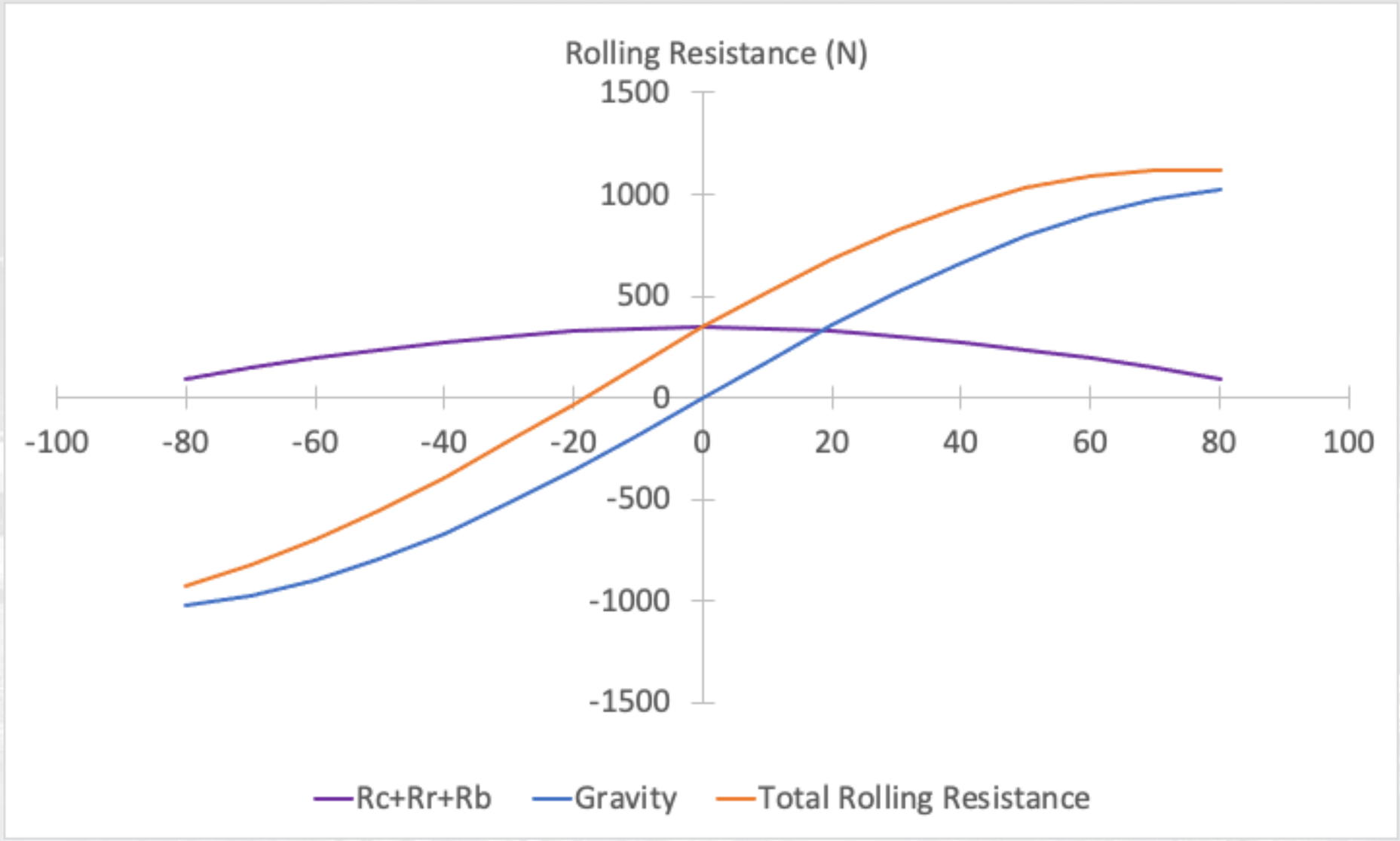
$$z = \left(\frac{3}{2}\frac{W_w \cos\theta}{(k_c + bk_\phi)\sqrt{D}}\right)^{\frac{2}{3}}$$

Bulldozing equation on pg. 43 is unchanged, but solution is altered by changing value of $z$

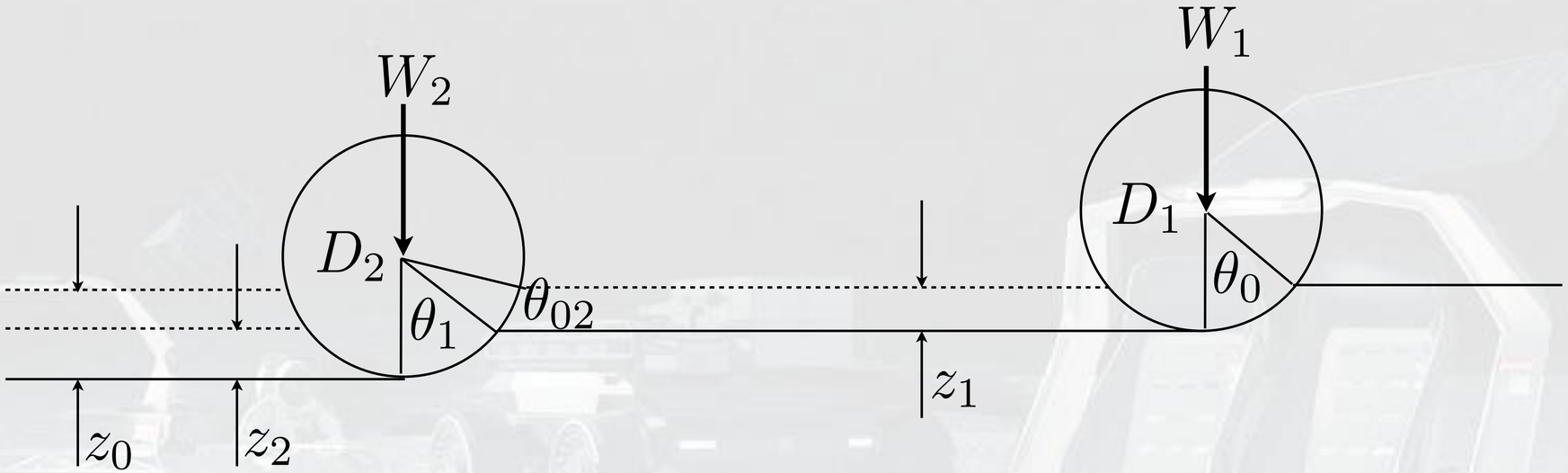
# Slope Effects on LRV Rolling Resistance



# Slope Effects on Rolling Resistance



# Tandem Wheels




$$z_0 = z_1 + z_2$$

$$\text{Assume } n = \frac{1}{2} \Longrightarrow P = k\sqrt{z}$$

$$P_1 = k\sqrt{z_1} \qquad P_2 = k\sqrt{z_1 + z_2}$$

# Soil Weight Bearing Analysis

In general,

$$W = \int_0^{\theta_0} dF \cos\theta = \int_0^{\theta_0} Pb\ ds \cos\theta$$

$$W = \int_0^{\theta_0} bk\sqrt{z} \cos\theta\ ds$$

$$ds = r\ d\theta \qquad z = r(\cos\theta - \cos\theta_0)$$

$$W = \int_0^{\theta_0} bkr\sqrt{r(\cos\theta - \cos\theta_0)} \cos\theta\ d\theta$$

# Generic Wheel Soil Suspension

Assuming small sinkage,

$$z \rightarrow \text{ small}, \theta \rightarrow \text{ small},$$

$$\cos\theta \approx 1 \qquad \cos\theta \; d\theta \approx d\theta$$

$$\cos\theta \approx 1 - \frac{\theta^2}{2} + (\text{higher order terms})$$

$$W = \frac{bkr^{3/2}}{\sqrt{2}} \int_0^{\theta_0} \sqrt{\theta_0^2 - \theta^2} \; d\theta$$

$$W = \frac{bkr^{3/2}}{\sqrt{2}} \frac{1}{2} \left[ \theta_0^2 \sin^{-1}\left(\frac{\theta}{\theta_0}\right) + \theta\sqrt{\theta_0^2 - \theta^2} \right]_0^{\theta_0}$$

# Weight on the Front Wheel

$$W = \frac{\pi b k r^{3/2}}{4\sqrt{2}}\theta_0^2$$

$$\text{Front wheel: } z_1 = r_1 - r_1\cos\theta_0$$

$$z_1 = r_1 - r_1\left(1 - \frac{\theta_0^2}{2} + \cdots\right) \implies \theta_0^2 \cong 2\frac{z_1}{r_1}$$

$$\boxed{W_1 \cong \frac{\pi b k z_1 \sqrt{r_1}}{2\sqrt{2}}}$$

# Weight on Back Wheel

Change to limits of integration:

$$0 \longrightarrow \theta_0, \quad r \longrightarrow r_2$$

$$W_2 = \frac{bkr_2^{3/2}}{\sqrt{2}} \int_0^{\theta_0} \sqrt{\theta_{02}^2 - \theta^2}\, d\theta$$

$$\sqrt{\theta_{02}^2 - \theta^2} \cong \theta_{02} \left(1 - \frac{1}{2}\frac{\theta^2}{\theta_{02}^2} + \cdots\right)$$

$$\int_0^{\theta_0} \sqrt{\theta_{02}^2 - \theta^2}\, d\theta \cong \theta_{02}\theta_1 - \frac{1}{6}\frac{\theta_1^3}{\theta_{02}} = \theta_{02}\theta_1 \left(1 - \frac{1}{6}\frac{\theta_1^2}{\theta_{02}^2}\right) \cong \theta_{02}\theta_1$$

# Weight on Back Wheel

$$W_2 = \frac{bkr^{3/2}}{\sqrt{2}}\theta_{02}\theta_1$$

$$z_0 \cong r_2\frac{\theta_{02}^2}{2} \qquad z_2 \cong r_2\frac{\theta_1^2}{2}$$

$$\theta_{02} \cong \sqrt{2\frac{z_0}{r_2}} \qquad \theta_1 \cong \sqrt{2\frac{z_2}{r_2}}$$

$$\boxed{W_2 = bk\sqrt{2r_2}\sqrt{z_0 z_2}}$$

# Track Depth of Tandem Wheels

$$\text{Front: } z_1 = \frac{2\sqrt{2}W_1}{\pi bk\sqrt{r_1}}$$

$$\text{Back: } z_2 = \left[\frac{W_2}{bk\sqrt{2r_2}}\frac{1}{\sqrt{z_0}}\right]^2$$

$$z_0 = z_1 + z_2 = \frac{2\sqrt{2}W_1}{\pi bk\sqrt{r_1}} + \frac{W_2^2}{(bk)^2 2r_2}\frac{1}{z_0}$$

Much algebra then ensues...

$$z_0^2 - \frac{2\sqrt{2}W_1}{\pi bk\sqrt{r_1}}z_0 + \frac{W_2^2}{(bk)^2 2r_2} = 0$$

# Rolling Resistance of Tandem Wheels

Solve the quadratic equation to get

$$z_0 = \frac{1}{bk}\left(\frac{\sqrt{2}W_1}{\pi\sqrt{r_1}} + \sqrt{\frac{2W_1^2}{\pi^2 r_1} + \frac{W_2^2}{2r_2}}\right)$$

This was all done for $n = \frac{1}{2} \implies R = \frac{2}{3}bkz_0^{3/2}$

$$R = \frac{2}{3}\frac{1}{\sqrt{bk}}\left(\frac{\sqrt{2}W_1}{\pi\sqrt{r_1}} + \sqrt{\frac{2W_1^2}{\pi^2 r_1} + \frac{W_2^2}{2r_2}}\right)^{3/2}$$

$$R = \frac{2}{3}\frac{1}{\sqrt{bk}}\left(\frac{2W_1}{\pi\sqrt{D_1}} + \sqrt{\frac{4W_1^2}{\pi^2 D_1} + \frac{W_2^2}{D_2}}\right)^{3/2}$$

# Nondimensional Forms

Total wheel load $W = W_1 + W_2$ Wheel weight ratio $a \equiv \frac{W_1}{W_2}$

$$\text{For } W_1 = W_2 = \frac{W}{2} \implies a = 1$$

$$W_1 = \frac{a}{1+a}W \quad W_2 = \frac{1}{1+a}W$$

$$R = \frac{2}{3}\frac{1}{(a+1)^{3/2}}\frac{W^{3/2}}{\sqrt{bk}}\left(\frac{2a}{\pi\sqrt{D_1}} + \sqrt{\frac{4a^2}{\pi^2 D_1} + \frac{1}{D_2}}\right)^{3/2}$$

Define wheel diameter ratio $\rho \equiv \frac{D_1}{D_2}$

# Nondimensional Forms

$$R = \frac{2}{3}\frac{1}{(a+1)^{3/2}}\frac{W^{3/2}}{D_2^{3/4}\sqrt{bk}}\left(\frac{2a}{\pi\sqrt{\rho}} + \sqrt{1+\frac{4a^2}{\pi^2\rho}}\right)^{3/2}$$

$$\text{Let } \xi \equiv \frac{2}{3}\frac{1}{(a+1)^{3/2}}\left(\frac{2a}{\pi\sqrt{\rho}} + \sqrt{1+\frac{4a^2}{\pi^2\rho}}\right)^{3/2}$$

$$\boxed{R = \frac{\xi}{\sqrt{bk}}\frac{W^{3/2}}{D_2^{3/4}}}$$

# Simple Example Case

Consider $\rho = 1 \quad (D_1 = D_2 = D)$

$$a = 1 \quad \left( W_1 = W_2 = \frac{W}{2} \right)$$

For tandem wheels, $R = \dfrac{0.580}{\sqrt{bk}} \dfrac{W^{3/2}}{D_2^{3/4}}$

For single wheel (n=1/2), $R = \dfrac{0.876}{\sqrt{bk}} \dfrac{W^{3/2}}{D_2^{3/4}}$

Tandem wheels reduce rolling resistance by 34%

# Dual Wheels

Equivalent to single wheel case twice as wide $b \Longrightarrow 2b$

$$R = \frac{0.876}{\sqrt{2}} \frac{1}{\sqrt{bk}} \frac{W^{3/2}}{D_2^{3/4}}$$

$$R_{dual} = \frac{0.619}{\sqrt{bk}} \frac{W^{3/2}}{D_2^{3/4}}$$

Dual wheel rolling resistance 29% less than single,

7% higher than tandem

But all of this assumes $n = 1/2$...

# Equations for Compression Resistance

$$z = \left[ \frac{3W_w}{(3-n)bk\sqrt{D}} \right]^{\frac{2}{2n+1}}$$

$$W_w = \text{weight on wheel}$$

$$D \equiv \text{wheel diameter}$$

$$R_c = \left( \frac{bk}{n+1} \right) z^{n+1}$$

$$R_c = \text{compression resistance (per wheel)}$$

# LRV Sinkage in Lunar Regolith

$$z = \left[ \frac{3W_w}{2\left(k_c + bk_\phi\right)\sqrt{D}} \right]^{\frac{2}{3}}$$

$$z_1 = 1.51\ cm$$

Back wheel is a tandem wheel

$$W_w = \frac{2}{3}\left(k_c + bk_\phi\right)\sqrt{D}z^{\frac{3}{2}}$$

# Tandem Wheels, n=1

$$W_i = \frac{2}{3}\left(k_c + bk_\phi\right)\sqrt{D}\left(z_i^{\frac{3}{2}} - z_{i-1}^{\frac{3}{2}}\right)$$

We already calculated $z_1 = 1.51\ cm$

$$W_2 = \frac{2}{3}\left(k_c + bk_\phi\right)\sqrt{D}\left(z_2^{\frac{3}{2}} - z_1^{\frac{3}{2}}\right)$$

$$z_2 = \left[\frac{3}{2}\frac{W_2}{\left(k_c + bk_\phi\right)\sqrt{D}} + z_1^{\frac{3}{2}}\right]^{\frac{2}{3}} = 2.443\ cm$$

This is the total depth (from undisturbed soil) of wheel 2

# Compaction Resistance, n=1

$$R_c = \frac{1}{2}(k_c + bk_\phi)z^2$$

$$R_c = 56.92\ N\ \text{(per side)} \Longrightarrow$$

$$R_c = 113.8\ N$$

# Or, You Could Cheat…

Approximation formulas for n=1

Two wheels in tandem

$$R_c = \frac{1.7}{2}\left(k_c + bk_\phi\right) z_1^2$$

Three wheels in tandem

$$R_c = \frac{2.3}{2}\left(k_c + bk_\phi\right) z_1^2$$

$z_1$ is the sinkage depth of the front wheel in both cases

$R_g,\ R_f$ are straightforward