Terramechanics 2: Traction

- Slip
- Grousers
- Drawbar Pull



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Shearing Strength of Soil

We want to know the maximum shear stress the soil can accommodate to find maximum tractive force of wheel

 $\tau \equiv$ shearing resistance per unit area

 $\tau = c_0 + \sigma t t$

 $\sigma \equiv \text{normal stress on the soil}$

 $H_0 \equiv \text{ideal soil thrust}$

 $H_0 = Ac_0 + W \tan \phi$



$$\operatorname{an}\phi = c_0 + \frac{W}{A}\tan\phi$$



Wheel Slip Ratio

- The difference is slip ratio: $s \equiv 1 \frac{V}{M}$
- If $\omega r = V$ then s = 0
- If $\omega r > V$ then 0 < s < 1
- If $\omega r \gg V$ (or V = 0) then s = 1
- If $\omega r < V$ (deceleration) then -1 < s < 0
- New definition becomes $s_d = \frac{\omega r}{1} 1$



• Wheel circumferential speed ωr will never exactly match vehicle speed

Wr



Tractive Force per (Smooth) Wheel

- $H = (Ac + W \tan \phi)$ $A = \text{area of contact} = b\ell$ c = soil cohesion $\phi = \text{soil angle of internal friction}$ s = wheel slip ratio K =shear deformation modulus
 - $\ell = \text{length of con}$



$$b\left[1-\frac{K}{s\ell}\left(1-e^{\frac{-s\ell}{K}}\right)\right]$$

ntact patch =
$$\frac{D}{2} \cos^{-1} \left(1 - \frac{2z}{D} \right)$$



Shear Deformation Modulus

- Wheel drives in regolith...
- Regolith particles around the contact area are sheared by the rotational and sideslip motions of the wheel, and...
- The shear stress develops based on the displacement of the regolith • Shear stress increases with increasing shear displacement
- Shear deformation modulus is a parameter of the surface and is determined experimentally
- Typically K=1.8 cm





Shear displacement j

From Hiroaki Inotsume, "Analysis of Angle of Attack for Efficient Slope Ascent by Rovers" CMU-RI-TR-15-22, Carnegie Mellon University, August 2015



Grousers (on Tracked Vehicle)





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Grousers (MSL Wheels)









Mars Rover Wheels





ENAE 788X - Planetary Surface Robotics

Terramechanics Test Rig (CMU)



K. Skonieczny, S. Moreland, and D. Wettergreen, "A Grouser Spacing Equation for Determining Appropriate Geometry of Planetary Rover Wheels" 2012 IEEE/RSJ International (Robots and Systems



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Terramechanics Test Rig (CMU)

Deadweight as payload –

> Free to translate vertically

Glass at wheel center plane

Subsurface soil particles and rim imaged

K. Skonieczny, S. Moreland, and D. Wettergreen, "A Grouser Spacing Equation for Determining Appropr Robots and Systems



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Wheel sinkage measurement

Load cell for drawbar pull measurement

Half-width wheel pressed against glass

ate Geometry of Planetary Rover Wheels" 2012 IEEE/RSJ International



Soil Flow Visualization

Flow velocity magnitude

Shear interface

Flow direction

K. Skonieczny, S. Moreland, and D. Wettergreen, "A Grouser Spacing Equation for Determining Appropriate Geometry of Planetary Rover Wheels" 2012 IEEE/RSJ International Robots and Systems



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Periodic Soil Shearing by Grousers



K. Skonieczny, S. Moreland, and D. Wettergreen, "A Grouser Spacing Equation for Determining Appropriate Geometry of Planetary Rover Wheels" 2012 IEEE/RSJ International Robots and Systems



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Soil Flow with 16 Grousers







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Soil Flow with 48 Grousers

K. Skonieczny, S. Moreland, and D. Wettergreen, "A Grouser Spacing Equation for Determining Appropriate Geometry of Planetary Rover Wheels" 2012 IEEE/RSJ International Robots and Systems



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Soil Excavation by Grousers



K. Skonieczny, S. Moreland, and D. Wettergreen, "A Grouser Spacing Equation for Determining Appropriate Geometry of Planetary Rover Wheels" 2012 IEEE/RSJ International (Robots and Systems UNIVERSITY OF MARYLAND

Wheel Parameters

K. Skonieczny, S. Moreland, and D. Wettergreen, "A Grouser Spacing Equation for Determining Appropriate Geometry of Planetary Rover Wheels" 2012 IEEE/RSJ International (Robots and Systems

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 \mathcal{Z}

 \mathcal{U}

Minimum Grouser Condition

 $t_{grouser\ contact} \leq t_{rim\ contact}$

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Geometric Derivation of Grouser Spacing

$$\begin{aligned} \overline{AC} &= \sqrt{(r+h)^2 - (r-z)^2} \quad \overline{AB} = \sqrt{r^2 - (r-z)^2} \\ \overline{BC} &= \overline{AC} - \overline{AB} = \Delta x \\ \psi &\leq \frac{1}{r(1-s)} \left[\sqrt{(1+h)^2 - (1-z)^2} - \sqrt{1 - (1-z)^2} \right] \\ \psi &\leq \frac{1}{(1-s)} \left[\sqrt{\left(1 + \frac{h}{r}\right)^2 - \left(1 - \frac{z}{r}\right)^2} - \sqrt{1 - \left(1 - \frac{z}{r}\right)^2} \right] \\ \psi &\leq \frac{1}{(1-s)} \left[\sqrt{\hat{h}^2 + 2\hat{h} + 2\hat{z} - \hat{z}^2} - \sqrt{2\hat{z} - \hat{z}^2} \right] \end{aligned}$$

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Required Grouser Spacing

Number of Grousers in Ground Contact

 $r = 40.6 \ cm$ Number of grousers = NAngle between grousers $\equiv \psi = \frac{2\pi}{N}$ LRV example: choose N = 16 $N_q = 1.3 \approx 1$

 $z = 1.812 \ cm$ Distance between grousers $\equiv \ell_g = \psi r = \frac{2\pi r}{N}$ Number of grousers in ground contact $\equiv N_g = \frac{2\pi r}{N\ell}$

Tractive Force per Wheel (With Grousers) $H = \left| b\ell c \left(1 + \frac{2h}{h} \right) N_g + W \tan \phi \left(1 + 0.64 \frac{h}{h} \arctan \frac{b}{h} \right) \right| \left| 1 - \frac{K}{s\ell} \left(1 - e^{-\frac{s\ell}{K}} \right) \right|$ $A = \text{area of contact} \cong b\ell$ $c = \text{soil cohesion} = 0.017 \text{ N/cm}^2$ $\phi = \text{soil angle of internal friction} = 35^{\circ}$ s = wheel slip ratio (typ. 0.02-0.05) $K = \text{shear deformation modulus} = 1.8 \ cm$ $\ell = \text{length of contact patch} = \frac{D}{2} \cos^{-1} \left(1 - \frac{2z}{D} \right)$ h = height of grouser N_q = number of grousers in contact with ground All values typical for lunar soil UNIVERSITY OF MARYLAND

Terramechanics 2: Traction

Effect of Slip Ratio on Wheel Thrust

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Basic Equation of Vehicle Propulsion DP: Drawbar pull (residual drive force)

- H: Maximum tractive force of wheels
- R_c: Compaction resistance
- R_b: Bulldozing resistance
- R_g: Gravitational resistance
- R_r: Rolling resistance (internal)

$DP = H - (R_c + R_b + R_g + R_r)$

Drawbar Pull vs. Slip (per wheel)

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-0.2

Some Notes on Terramechanics

- This is the simplest approach to calculating wheel-soil interactions
- Real-world issues not modeled include
 - Non-homogeneities
 - Soil layering
 - Soil transport under wheel
- This technique is conservative in estimating drawbar pull
- more to come

• Braking is more complicated than sticking s < 0 into the equation for H

